FLUCTUATING ASYMMETRY OF ANTLERS OF WHITE-TAILED DEER (*ODOCOILEUS VIRGINIANUS*) IN RELATION TO YEARLING ANTLER EXPRESSION

THESIS

Presented to the Graduate Council of
Southwest Texas State University
in Partial Fulfillment of
the Requirements

For the Degree

Master of SCIENCE

By

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San Marcos, Texas
December 2001

ACKNOWLEDGEMENTS

I thank my parents Larry and Sherry Pruitt for their unending support of me through my college career and my life. Without their constant and unconditional reassurance, completing this thesis would have been nearly impossible for me.

I also thank my committee members. Dr. Simpson has shared invaluable knowledge of wildlife. Dr. Ott has been constant in making my scientific thoughts truly meaningful. Finally, I owe a great debt of gratitude to Dr. Baccus for his guidance through all portions of this thesis and for his large efforts to help move me forward when things seemed to get bogged down.

I thank Dr. Prahbakaran for giving me a teaching position throughout the time that I was working on this thesis.

I thank the Kerr Wildlife Management Area for providing me access to the antlers that were used in this study. I specifically thank Gene Fuchs for his effort in helping to fill holes in my data.

I thank the many graduate students that came before me and made measurements that I used in this study.

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ABSTRACT

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Fluctuating asymmetry is a measure of differences in bilateral traits within individuals and has been linked to heterozygosity, an individual's ability to cope with environmental stresses, and mate choice. Many studies have suggested that fluctuating asymmetry could be a signaling trait for intrasexual interactions and for sexual selection in cervid species. Additionally antler characteristics throughout life have been shown to be smaller in bucks that were spike-antlered as yearlings than in bucks that were fork-antlered as yearlings. Here the asymmetry of main beam length, total normal tine length, total abnormal tine length, total tine length, gross Boone and Crockett scores, antler weight, and main beam circumference are compared for the first 4 sets of antlers for 144 bucks born between 1973 and 1990 at the Donnie Harmel Research Facility at the Kerr Wildlife Management Area. Comparisons were performed using Levene's test and linear regression to test if bucks that were spike-antlered as yearlings are more asymmetric throughout life than bucks that were fork-antlered (3 or more points) as yearlings. Significant differences were found for variance in asymmetries based on deer age, yearling antler type and the interaction of yearling antler type and deer age. No difference was found in the regression slopes of variance in asymmetries versus deer age between yearling antler types. Bucks that were fork-antlered as yearlings had a smaller variance in asymmetry than bucks that were spike-antlered as yearlings. The age of bucks also played a role in asymmetry differences, with 1-year old deer having the largest variance in asymmetry of antler traits for both antler types. These results suggest bucks that were spike-antlered as yearlings may be less heterozygous than bucks that were fork-antlered as yearlings, and thus asymmetry in antler traits may function in signaling.

INTRODUCTION

Fluctuating asymmetry is a measure of small, random differences that occur between the right and left sides of bilateral characteristics (Merila and Bjorklund 1995). This measure is interpreted as inefficiencies in the developmental processes that buffer against environmental perturbations (Van Valen 1962). These differences can result from environmental deficiencies, such as lack of nutrition, parasites, and physical injuries, or genetic deficiencies that hamper the buffering processes (Moller 1997).

Fluctuating asymmetry in many species exhibits a negative relationship with heterozygosity, suggesting that more heterozygous individuals are better able to buffer against environmental perturbations (Palmer and Strobeck 1986). Additionally, there is a negative relationship between fluctuating asymmetry and fitness components in an individual or population (Moller 1997). Because of these relationships, Palmer (1996) suggested that fluctuating asymmetry could be used as a tool to infer both individual and population health for many species.

Studies of fluctuating asymmetry of antler characteristics in cervids are consistent with the predictions of the theory of fluctuating asymmetry and actual fluctuating asymmetry for other groups of organisms. In roe deer (*Capreolus capreolus*), Pelabon and Van Breukelen (1998) discovered that fluctuating asymmetry increased as population densities increased and as individual health decreased, suggesting that fluctuating asymmetries can indicate individual quality and population health. Markusson and

Folstad (1997) found a negative relationship between the parasitic load of an animal and fluctuating asymmetries of antlers, but no significant relationship between the overall health indices and antler asymmetries in reindeer (*Rangifer tarandus*). Baccus and Welch (1982) attributed fluctuating asymmetry of sika deer (*Cervus nippon*) antlers in central Texas to both developmental processes and genetic factors, including possible inbreeding. The results of a study of moose (*Alces alces*) indicated that fluctuating asymmetry in antler points did not signal the quality of the animal as inferred by body weight (Solberg and Saether 1993). However, there was an age dependent correlation between antler size and fluctuating asymmetry (Solberg and Saether 1993). Davis (1982) determined that antler asymmetry was induced by limb amputation in Sambar deer (*Cervus unicolor*).

Ditchkoff et al. (2001) tested whether asymmetry in white-tailed deer (*Odocoileus virginianus*) antlers followed the pattern for a sexually selected trait predicted by Moller (1992). It was determined that absolute asymmetry (asymmetry not scaled for size) did not follow the predicted pattern, but relative fluctuating asymmetry (asymmetry scaled for size) did follow the predicted pattern of decreased asymmetry with increased antler size (Ditchkoff et al. 2001). The negative relationship of relative asymmetry and antler size was attributed to the increased ability of large-antlered deer to cope with environmental conditions (Ditchkoff et al. 2001). Lower asymmetries were also found for individuals with greater body weight. From these finding, they suggested that individuals with lower asymmetry values would have greater individual quality (Ditchkoff et al. 2001). A positive relationship between absolute asymmetry and antler size was also discovered; thus suggesting that relative asymmetry would be a better indicator of true quality (Ditchkoff et al. 2001).

The idea of asymmetry as a tool in evaluating the "quality" of white-tailed deer antlers is not inconsistent with other methods. One of the most popular methods for evaluating antlers of white-tailed deer by hunters is the Boone and Crockett scoring system. This scoring system is based on the summed measurements of various components of deer antlers, including tine lengths, main beam lengths, antler circumferences, and inside spread for a set of antlers. However, in the official scoring system, deductions are taken from the overall score based on differences in the right and left sides of a set of antlers (Boone and Crockett 1999). Thus a deer with symmetric antlers will have a higher Boone and Crockett score than a deer with similar, but asymmetric antlers.

Fluctuating asymmetry could serve as a signaling device in sexual selection and mate selection (Moller 1992, Markusson and Folstad 1997, Moller and Thornhill 1998, Pelabon and Van Bruekeland 1998, Ditchkoff et al. 2001). The theory can be stated as individuals with the most symmetric signaling traits are the best equipped to cope with environmental stresses. Also because of the extreme cost of these traits, only the best individuals will produce both large and symmetric antlers (Moller 1992). Because of this, individuals with symmetric secondary sexual traits should be selected for in most mating systems. Moller and Thornhill (1998) found that this type of negative relationship between mating success and fluctuating asymmetry as a signaling trait, with mating success increasing with decreasing asymmetry, held true in most studies on fluctuating asymmetry and sexual selection.

Since antlers in white-tailed deer are secondary sexual traits, fluctuating asymmetry of antlers may function in the mating preferences of females. This is of special interest if fluctuating asymmetry can be linked to the heterozygosity of the individual (Palmer and Strobeck 1986). Because it also has been suggested that antler quality is linked with heterozygosity of a deer (Scribner et al. 1989), the question arises about the relationship of antler quality and fluctuating asymmetry with regard to an individual buck's antler quality and possibly to sexual selection.

Many factors contribute to the ultimate expression of antler characteristics in white-tailed deer. The age of a deer, various environmental factors, and genetics all contribute to the ultimate expression (Harmel 1983, Scribner et al. 1989, Harmel et al. 1989). Most antler characteristics show a curvilinear relationship with age, with most increasing in size until 4.5 to 5.5 years of age (Scribner et al. 1989, Demarais 1998).

The interaction of environmental and genetic factors is of particular interest in the management of white-tailed deer. Harmel et al. (1989) found a direct relationship between the quality of diet and the size of antlers produced by bucks. A minimal protein requirement of 9.9% crude protein in the diet has been demonstrated for proper antler production in white-tailed deer (Asleson et al. 1996). However, Asleson et al. (1997) also suggested that short-term protein restriction does not significantly contribute to long-term antler characteristics in deer older than two years.

Environmental factors other than nutrition also contribute to the formation of antlers. Photoperiod has been shown to affect antler development in white-tailed deer fawns (Verme 1988) and adult white-tailed deer bucks (Goss 1983). The dominance rank of a buck has been shown to affect the timing of events in the antler cycle of individual bucks (Forand et al. 1985). Antler characteristics are also affected by injuries that a buck may sustain during antler production (Goss 1983).

Genetic factors also influence antler characteristics. There are, however, significant disagreements over the extent of influence that genetics has on antler characteristics when compared to other factors (Demarais 1998). Scribner et al. (1989) found that deer with higher levels of heterozygosity where able to maintain higher levels of antler development. A positive relationship existed between heterozygosity and main beam length and diameter and overall antler size of bucks (Scribner et al. 1989).

A study conducted from 1973-1985 at the Kerr Wildlife Management Area, Kerr County, Texas examined the question of genetic influence on antler characteristics using heritability estimates. The study involved 138 pen-raised bucks and 505 sets of antlers. From this study, heritability estimates for weight, main beam length, antler weight, basal circumference, inside spread, and total points showed that antler characteristics and body weight were highly heritable characters for all age classes (Harmel et al. 1983, William et al. 1994). Lukefahr (1997) asserted that the heritability estimates of antler characteristics in the Williams et al. (1994) study overestimated heritability and that heritability actually was extremely low in that study, attributing differences in analyses primarily to differences in the birth date of individual animals. Additionally, a study conducted on pen-raised deer from 1977 to 1993 at Mississippi State University facilities assigned low to moderate levels of heritability to antler characteristics in white-tailed deer (Lukefahr and Jacobson 1998).

Ott et al. (1998) examined the antler development of white-tailed deer with respect to the type of antlers pen-raised bucks produced as yearlings. This study was specifically concerned with the usefulness of yearling antlers in predicting the quality of antlers produced at maturity (4.5-years of age). Clear differences were found between antler size and characteristics for 4.5-year old deer that had spike-antlers as yearlings or fork-antlers as yearlings. There was also a high correlation between the antler size of yearling bucks and the antler size of 4.5-year old bucks. (Ott et al. 1998) This suggests that yearling antler type can be used to predict the antler quality of bucks throughout life.

If both fluctuating asymmetry and antler quality are related to the heterozygosity of bucks, then it can be predicted that animals of poorer antler quality will have a higher fluctuating asymmetry throughout life. Since fluctuating asymmetry is expected to decrease with age due to decreasing developmental demands, it can also be predicted that the fluctuating asymmetry of poorer quality, and thus, less heterozygous individuals, would decrease at a slower rate than that of higher quality individuals.

Ott et al. (1998) demonstrated that bucks that were spike-antlered as yearlings have poorer antler quality through the first four sets of antlers than deer that were fork-antlered as yearlings. With this knowledge, it can be predicted that the fluctuating asymmetry of spike-antlered yearlings will be greater than that of fork-antlered yearlings and the change in asymmetry with age will decrease slower in bucks that were spike-antlered as yearlings than in bucks that were fork-antlered as yearlings. Since fluctuating asymmetry is largely independent of direct genetic effects affecting its expression (Palmer 1996), these differences can be attributed to environmental conditions and indirect genetic effects, such as heterozygosity, that affect the ability of an individual animal to cope with the environmental conditions. This study tests the predictions that fluctuating asymmetry in antlers of bucks that were spike-antlered as yearlings is greater than the fluctuating asymmetry in antlers of bucks that were fork-antlered as yearlings for various antler characteristics and that the fluctuating asymmetry of bucks that were spike-antlered as yearlings decreases at a slower rate with age than does the fluctuating asymmetry of bucks that were fork-antlered as yearlings using bucks that were exposed to nearly identical environmental conditions, emphasizing the indirect genetic effects on fluctuating asymmetry.

METHODS

The data set used in this study was composed of the antlers from 144 male white-tailed deer studied by Ott et al. (1998). These deer were born between 1973 and 1990 in a closed herd and were pen-raised in the Donnie Harmel Reseach Facility at the Kerr Wildlife Management Area, a facility owned and operated by Texas Parks and Wildlife Department. Water and pelleted rations with 18 % protein were available ad libitum (Harmel et. at 1989). As much as possible, all deer were exposed to the same environmental conditions. For all deer, body weight, antler spread, antler weight, number of points, basal circumference, and main beam length measurements were recorded after the development of antlers. Bucks included in this study lived through at least the development of the first four sets of antlers. Antler types were classified based on the type of antlers produced in the first set of antlers by a buck. These were fork-antlered as a yearling (SAY bucks) or spike-antlered as a yearling (SAY bucks).

Antlers were measured for components of Gross Boone and Crockett scores as in the Ott et al (1998) study. Measurements for Gross Boone and Crockett score included main beam length (MB), 4 main beam circumference measurements (H), lengths of all normal tines (G) and abnormal tines (AB), and inside spread. See appendix A for illustration of Gross Boone and Crockett measurements. Gross Boone and Crockett scores were then computed for each set of antlers for all deer. Scores were computed as follows:

$$GBC = \Sigma MB_r + \Sigma MB_l + \Sigma G_{ri} + \Sigma G_{li} + \Sigma AB_{ri} + \Sigma AB_{li} + \Sigma H_{ri} + \Sigma H_{li} + SP$$

where GBC is the gross Boone and Crockett score, MB_r is the length of the right main beam, MB_l is the length of the left main beam, ΣG_{ri} is the sum of the lengths of all normal tines on the right side, ΣG_{li} is the sum of the lengths of all normal tines on the left side, ΣAB_{ri} is the sum of the lengths of all abnormal tines on the right side, ΣAB_{li} is the sum of the lengths of all abnormal tines of the left side, ΣH_{ri} is the sum of all main beam circumferences on the right side, ΣH_{li} is the sum of all main beam circumferences on the left side, and SP is the length of the greatest inside spread of the set of antlers. These measurements are the same as those used in official Boone and Crockett scoring without deductions taken for differences in the right and left side (Boone and Crockett 1999).

Using these data, asymmetry values for the 144 bucks were computed for antler weight, the sum of total tine lengths, the sum of normal tine lengths, the sum of abnormal tine lengths, the sum of the main beam circumference measures, main beam lengths, and the sum of GBC components for each side of a set of antlers. The sum of GBC components was as stated above for each side of the antlers, causing inside spread measurements to not factor into the analysis.

Because the absolute fluctuating asymmetry of antlers in white-tailed deer demonstrate a negative relationship with antler size (Ditchkoff et al. 2001), an asymmetry method that scales out character size was needed (Palmer and Strobeck 1986). Palmer and Strobeck (1986) suggested using a technique where the difference between the right and left characters (absolute asymmetry) were divided by the average of the right and left characters of an individual. This method was used in this study as stated by:

$$A = [(R_i - L_i) / ((R_i + L_i)/2)]$$

where R_i is the measurement of the right character and L_i is the measurement of the left character for a set of antlers. Asymmetry of total tine lengths and total normal tine lengths cannot be determined for 1.5-year-old spike-antlered yearlings due to an absence of tines. Because this was due to the study design, the asymmetries of total tine length and total normal tine length for 1.5-year-old SAY bucks were not used in further analysis.

Deer were categorized as spike or fork antler types and the age of the buck. The individual asymmetries measured were main beam asymmetry (MBA), total tine length asymmetry (TTA), total normal tine length asymmetry (TGA), total main beam circumferences asymmetry (THA), gross Boone and Crockett asymmetry (GBCA), antler weight asymmetry (AWA), and abnormal tine length asymmetry (APA).

A Kolmogorov-Smirnov test was performed to test for normality of all individual asymmetries. The means of the individual asymmetry measures were tested for differences from the predicted mean of zero for fluctuating asymmetry in bilateral traits using a t-test. Since all measures of asymmetry were not normal (Table 1), Levene's test was used to test for differences between variances of all individual asymmetries and age and antler type subgroups. This test handles non-normal data better than other tests of homogeneity of variance (Palmer and Strobeck 1986). Levene's test was used to test for differences in variance of asymmetries based upon yearling antler type, age of deer, and the interaction of yearling antler type and age of deer. Differences in variance based on yearling antler type only and age of deer only were also tested using Levene's test. If a difference in variance was shown by Levene's test, a modified Tukey-type test (Zar 1999) was used to separate subgroups of the asymmetry based on differences in variances.

Linear regression of the variance of the asymmetries versus the age of the deer was performed for all asymmetry measures separately. Regressions were performed separately for SAY bucks and FAY bucks. The regression slopes of SAY bucks were compared to the regression slopes of FAY bucks using a t-test (Zar 1999). All analyses was computed using an $\alpha = 0.05$ significance level and SPSS 9.0 and Excel worksheets.

RESULTS

The results of t-test for all asymmetry measures indicated that the means for all asymmetry measures showed no significant differences from zero (Table 1). For all asymmetry measures, there was a significant departure from normality within age classes (Table 2).

Table 1. The results of t-test for deviations from an expected mean of zero for mean asymmetry of antler traits of 144 bucks at the Kerr Wildlife Management Area. The means, standard deviations, t-values and significance values are shown in the table.

Trait	mean	s	t-value	sig.
MBA	5.136E-03	0.137	0.038	$p > 0.500$
TGA	-5.490E-02	0.498	-0.110	$p > 0.500$
TTA	-8.880E-02	0.477	-0.186	$p > 0.500$
THA	-2.160E-03	0.092	-0.024	$p > 0.500$
GBCA	-1.680E-02	0.114	-0.147	$p > 0.500$
AWA	-1.740E-03	0.188	-0.009	$p > 0.500$
APA	-2.069E-01	0.633	-0.327	$p > 0.500$

MBA- Main Beam

TGA- Total Normal Tine Length

TTA – Total Tine Length

THA – Total Main Beam Circumferences

AWA – Antler Weight

APA – Total Abnormal Tine Length

CGCA – Gross Boone & Crockett Score

Table 2. The results of Kolmogorov-Smirnov Test of normality for antler asymmetry by age class of 144 bucks at the Kerr Wildlife Management Area. The degrees of freedom, test statistic, and significance values are shown in the table.

Trait	Age	df	Statistic	p-value
MBA	1	141	0.214	0.000
	2	142	0.171	0.000
	3	141	0.078	0.034
	4	143	0.092	0.005
TGA	1	96	0.187	0.000
	2	130	0.168	0.000
	3	133	0.200	0.000
	4	143	0.214	0.000
TTA	1	96	0.194	0.000
	2	130	0.168	0.000
	3	133	0.200	0.000
	4	143	0.187	0.000
THA	1	136	0.128	0.000
	2	136	0.104	0.001
	3	134	0.052	0.200
	4	144	0.093	0.004
GBCA	1	136	0.150	0.000
	2	136	0.054	0.200
	3	134	0.116	0.000
	4	143	0.127	0.000
AWA	1	137	0.156	0.000
	2	141	0.133	0.000
	3	141	0.111	0.000
	4	140	0.102	0.001
APA	1	137	0.507	0.000
	4	144	0.416	0.000

MBA- Main Beam Length

TGA- Total Normal Tine Length

TTA – Total Tine Length

THA – Total Main Beam Circumferences

AWA – Antler Weight

APA – Total Abnormal Tine Length

CGCA – Gross Boone & Crockett Score

<u>Asymmetry Variances</u>

The results of Levene's test for homogeneity of variance showed significant departures from homogeneity for all asymmetry measures based on age, antler type and the interaction of age and antler type (Tables 3 and 4).

Table 3. The variances and sample sizes for all asymmetry measures and subgroups tested for antler traits of 144 bucks at the Kerr Wildlife Management Area.

		MBA		TGA		TTA		THA		GBCA		AWA		APA	
Subgroup		s^2	N	s^2	n	s^2	N	s^2	n	s^2	n	s^2	n	s^2	n
Deer Age	1	0.059	140	0.730	95	0.612	95	0.018	135	0.025	136	0.077	136	0 286	136
	2	0.009	141	0.133	129	0.133	129	0.007	135	0.009	136	0.013	140	0.000	135
	3	0.004	140	0.134	132	0.134	132	0.005	133	0.008	134	0.011	140	0.000	133
	4	0.004	142	0.123	142	0.100	142	0.004	143	0.011	143	0.008	139	0.921	143
Yearling Antler Type & Age Interaction	1*SAY	0.153	41	.	.	.	.	0.033	39	0.046	39	0.205	37	0.000	40
	2*SAY	0.018	42	0.267	36	0.267	36	0.010	42	0.009	42	0.021	42	0.000	42
	3*SAY	0.006	42	0.172	37	0.172	37	0.006	38	0.009	38	0.020	42	0.000	38
	4*SAY	0.005	43	0.204	42	0.204	42	0.003	43	0.012	43	0.011	42	0.412	43
	1*FAY	0.019	98	0.730	95	0.612	95	0.012	95	0.016	95	0.030	97	0.405	95
	2*FAY	0.005	98	0.080	92	0.080	92	0.006	92	0.009	92	0.009	97	0.000	92
	3*FAY	0.003	97	0.118	94	0.118	94	0.004	93	0.008	94	0.008	97	0.000	94
	4*FAY	0.004	98	0.080	99	0.056	99	0.005	99	0.011	98	0.014	96	1.004	99

SAY – Spike-antlered as a yearling

FAY – Fork-antlered as a yearling

MBA- Main Beam Length

TGA- Total Normal Tine Length

TTA – Total Tine Length

THA – Total Main Beam Circumferences

AWA – Antler Weight

APA – Total Abnormal Tine Length

CGCA – Gross Boone & Crockett Score

Table 4. The results from Levene's test of homogeneity of variances for all asymmetry measures and subgroups of antler traits of 144 bucks at the Kerr Wildlife Management Area. The test statistic, degrees of freedom, and significance are shown.

Trait	Subgroup	Levene	df1	df2	Sig.
MBA	Antler type*Age	6.979	7	512	0.000 ***
	Age	5.403	3	516	0.001 **
	Antler type	4.387	1	518	0.037 *
TGA	Antler type*Age	9.720	6	470	0.000 ***
	Age	15.721	3	473	0.000 ***
	Antler type	0.102	1	475	0.750
TTA	Antler type*Age	9.034	6	470	0.000 ***
	Age	14.849	3	473	0.000 ***
	Antler type	0.063	1	475	0.802
THA	Antler type*Age	4.556	7	512	0.000 ***
	Age	5.595	3	516	0.001 **
	Antler type	2.963	1	518	0.086
GBCA	Antler type*Age	3.015	7	512	0.004 **
	Age	2.992	3	516	0.031 *
	Antler type	0.590	1	518	0.443
AWA	Antler type*Age	11.862	7	510	0.000 ***
	Age	7.549	3	514	0.000 ***
	Antler type	7.717	1	516	0.006 **
APA	Antler type*Age	146.077	7	543	0.000 ***
	Age	36.689	1	279	0.000 ***
	Antler type	16.290	1	549	0.000 ***

* = 0.05, ** = 0.01, *** = 0.001

MBA- Main Beam Length

TGA- Total Normal Tine Length

TTA – Total Tine Length

THA – Total Main Beam Circumferences

AWA – Antler Weight

APA – Total Abnormal Tine Length

CGCA – Gross Boone & Crockett Score

Main Beam Asymmetry

The results of Levene's test for homogeneity of variance (Table 6) showed a difference in variance among the main beam asymmetry based on age, yearling antler type and the interaction of age and yearling antler type ($p < 0.001$). A difference in variance was also noted separately for age subclasses ($p < 0.001$) and yearling antler type subclasses ($p = 0.006$).

The results of a Tukey-type test indicated significant differences in the variance in the asymmetry of antlers of 1 and 2-year old deer from all other sets for main beam asymmetry. The variance in the asymmetry of age groups 3 and 4-year old showed no difference.

The variance for main beam asymmetry differed for the interaction of age and yearling antler type (Figure 1). The results indicate that antlers from 1-year old SAY bucks had the greatest variance ($s^2 = 0.153$) of all other interaction groups. It was also found that the variance in the asymmetry of antlers of 1-year old deer that were FAY bucks and 2-year old SAY bucks were similar to each other and significantly different from all other subgroups. All other subgroups had similar variances, with the variance in the asymmetry of the antlers of 3-year old deer that were FAY bucks ($s^2 = 0.003$) having the smallest variance.

Total Normal Tine Length Asymmetry

Total normal tine length asymmetry showed a difference in variance in asymmetry (Table 6) based on age, yearling antler type, and the interaction of age and

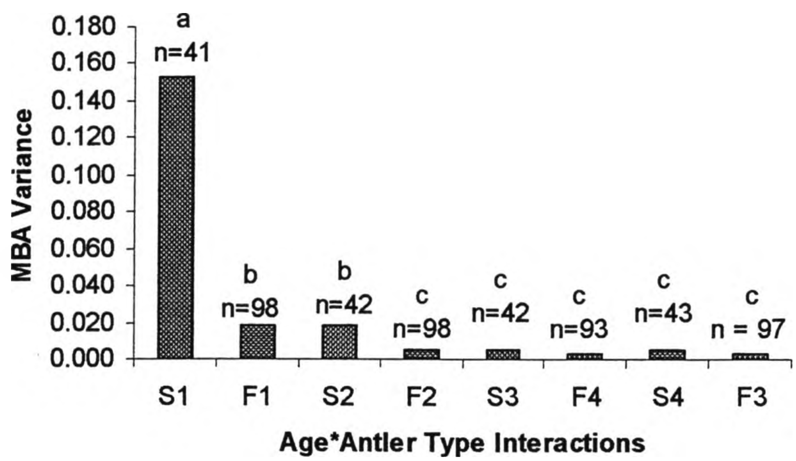

Figure 1. Variance in asymmetries for spike and fork-antlered white-tailed deer bucks for main beam length asymmetry (MBA) variances by age groups 1, 2, 3, and 4-years of age. Sample size and groupings are displayed.

yearling antler type ($p < 0.001$). A difference in variance was also noted separately for age ($p < 0.001$). There was no difference in variance based on the yearling antler type ($p = 0.719$).

Significant differences were found in the variance in total normal tine length asymmetry of the antlers from 1-year old deer ($s^2 = 0.730$) from all other sets of antlers. The variance in the asymmetry of antlers from 2, 3, and 4-year old deer were all similar, with the variance in the asymmetry of antlers from 4-year old deer ($s^2 = 0.123$) being the smallest.

The results of a Tukey-type test showed differences in the variance of total normal tine asymmetry for the interaction of age and yearling antler type (Figure 2). The asymmetry of antlers for 1-year old FAY bucks had a significantly larger variance ($s^2 =$

0.730) than all other interaction groups. SAY bucks formed a subgroup of 2, 3, and 4-year old bucks with similar variances. FAY bucks at ages 2, 3, and 4 had variances in asymmetry that were similar to that of 3-year old SAY bucks. The asymmetry of antlers for 2-year old FAY bucks had the smallest variance ($s^2 = 0.080$).

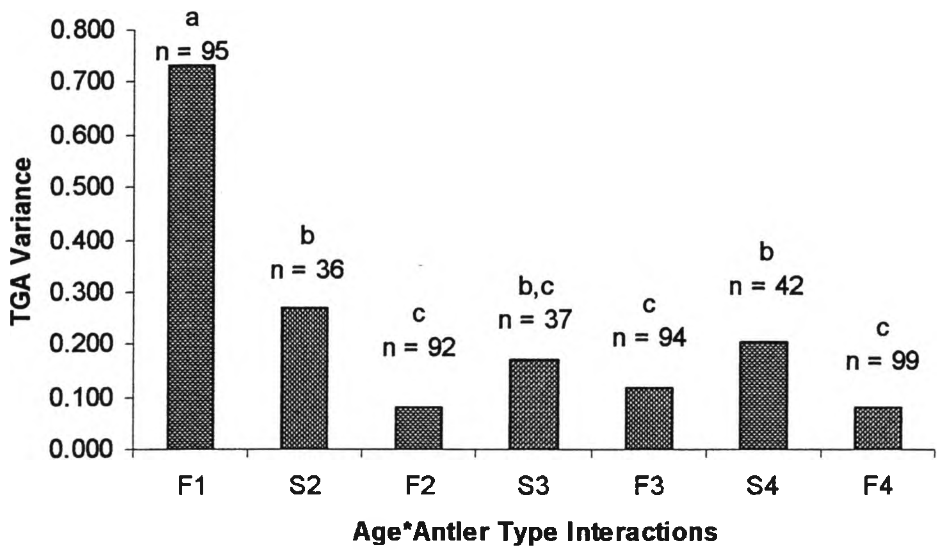

Figure 2. Variance in asymmetries for spike and fork-antlered white-tailed deer bucks for total normal tine length asymmetry (TGA) variances by age groups 1, 2, 3, and 4-years of age. Sample size and groupings are displayed.

Total Tine Length Asymmetry

A difference in variance (Table 6) was shown in the variance among the total tine length asymmetry based on age, yearling antler type, and the interaction of age and yearling antler type ($p < 0.001$) and separately for age ($p < 0.001$). No difference in variance was seen based on the yearling antler type ($p = 0.876$).

The variance ($s^2 = 0.612$) in total tine length asymmetry of the antlers of 1-year old FAY bucks differed significantly from all other sets of antlers. The variances in the asymmetry of deer at ages 2, 3, and 4-year old were similar, with the variance ($s^2 = 0.100$) in the asymmetry of antlers from 4-year old deer being the smallest.

The results of a Tukey-type test showed differences in the variance of total tine asymmetry for the interaction of age and yearling antler type (Figure 3). The asymmetry of antlers from 1-year old FAY bucks had a significantly larger variance ($s^2 = 0.612$) than all other interaction groups. SAY bucks at age 2, 3, and 4-years of age were similar, as were 3 and 4-year old SAY bucks and 3-year old FAY bucks. The asymmetries in total tine length of FAY bucks at 2 and 3-years old were similar to the asymmetry in 3-year old SAY bucks. The variance in asymmetry of 2 and 4-year old FAY bucks composed another subgroup, with the asymmetry of total tine length of 4-year old FAY bucks having the smallest variance ($s^2 = 0.056$).

Total Main Beam Circumference (H) Asymmetry

An examination of the effects of age, yearling antler type, and the interaction of age and yearling antler type on total main beam circumference asymmetry showed a difference in variance in the asymmetry ($p < 0.001$). A difference in variance was also noted separately for age ($p = 0.001$). There was no difference in variance based on the yearling antler type ($p = 0.076$).

Bucks at the 1-year old age class had a significantly larger variance ($s^2 = 0.018$) in total main beam circumference asymmetry than all other age classes. Similar variances

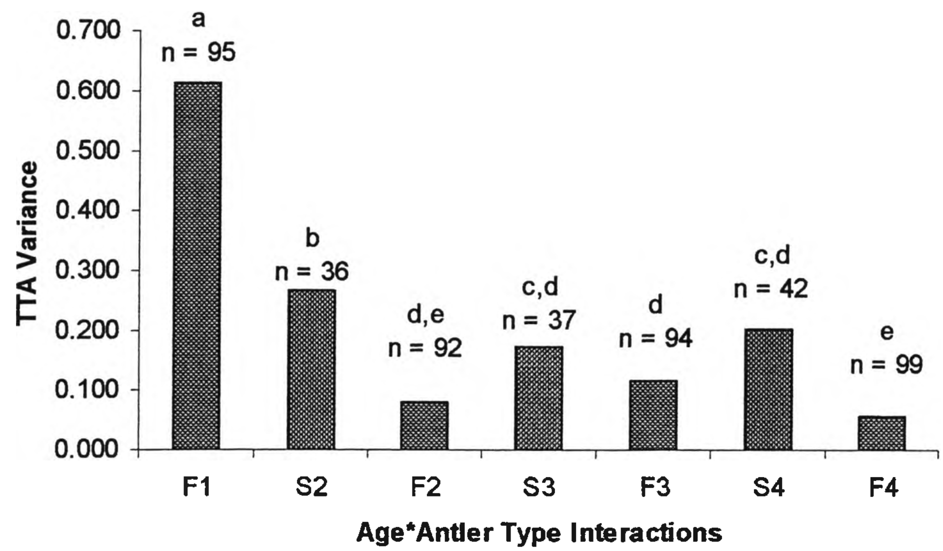

Figure 3. Variance in asymmetries for spike and fork-antlered white-tailed deer bucks for total tine length asymmetry (TTA) variances by age groups 1, 2, 3, and 4-years of age. Sample size and groupings are displayed.

were found in the asymmetry of antlers of 2 and 3-year old bucks, as was found between the variances in the asymmetries of antlers of bucks of 3 and 4-year old antlers. The variance in the asymmetry of antlers of 4-year old bucks ($s^2 = 0.004$) was the smallest.

The results of a Tukey-type test showed differences in the variance of total main beam circumference asymmetry for the interaction of age and yearling year type (Figure 4). The asymmetry of total main beam circumferences of 1-year old SAY bucks had a significantly larger variance ($s^2 = 0.033$) than all other interaction groups. SAY bucks at ages 2 and 3-year and FAY bucks at 1-year old had similar variances in asymmetry. The total main beam circumferences of SAY bucks at 2 and 3-year old and FAY bucks at 2 and 4-years old had similar variances in asymmetry. The variance in asymmetry of 3 and

4-year old SAY bucks and 2, 3, and 4-year old FAY bucks were similar, with the asymmetry in total main beam circumferences of 4-year old FAY bucks having the smallest variance ($s^2 = 0.003$).

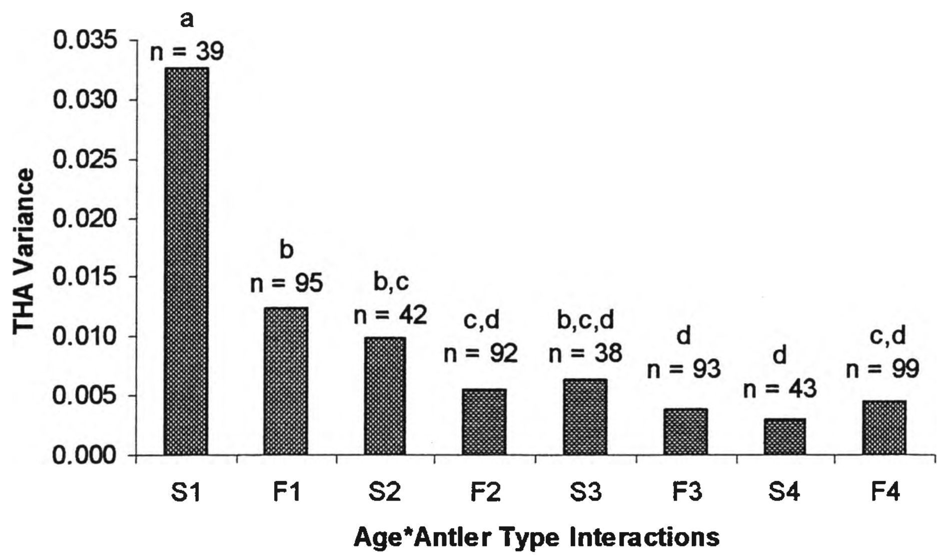

Figure 4. Variance in asymmetries for spike and fork-antlered white-tailed deer bucks for total main beam circumference asymmetry (THA) variances by age groups 1, 2, 3, and 4-years of age. Sample size and groupings are displayed.

Gross Boone and Crockett Asymmetry

Differences in variance of gross Boone and Crockett score asymmetry based on age, yearling antler type, and the interaction of age and yearling antler type (Table 6) were shown by Levene's test ($p = 0.002$). Age classifications also showed a difference in variance ($p = 0.004$). No difference was seen in the variance of asymmetry based on the yearling antler type ($p = 0.360$).

Gross Boone and Crockett score asymmetry of the first set of antlers for a buck had a larger variance than older age classes. There were no significant differences in the variances in the asymmetries of antlers for 2, 3, and 4-year old bucks with the variance in the asymmetry of gross Boone and Crockett scores for 3-year old bucks ($s^2 = 0.008$) being the smallest.

The asymmetry of antlers for 1-year old SAY bucks had a significantly larger variance ($s^2 = 0.046$) than all other interaction groups. There were no differences in variance in asymmetry of gross Boone and Crockett scores for SAY bucks at 2, 3, and 4-years of age and 1, 2, and 4-year old FAY bucks (Figure 5). The variances in the asymmetry of gross Boone and Crockett scores of SAY bucks at 2, 3, and 4-year old were similar to the variance in asymmetries of FAY bucks at 2, 3, and 4-years old. The smallest variance in asymmetry of gross Boone and Crockett scores ($s^2 = 0.008$) occurred in 3-year old FAY bucks.

Antler Weight Asymmetry

Antler weight asymmetry variance based on the age, yearling antler type, and the interaction of age and yearling antler type differed among classifications ($p < 0.001$). Variances also differed based separately on ($p < 0.001$) and yearling antler type ($p = 0.001$).

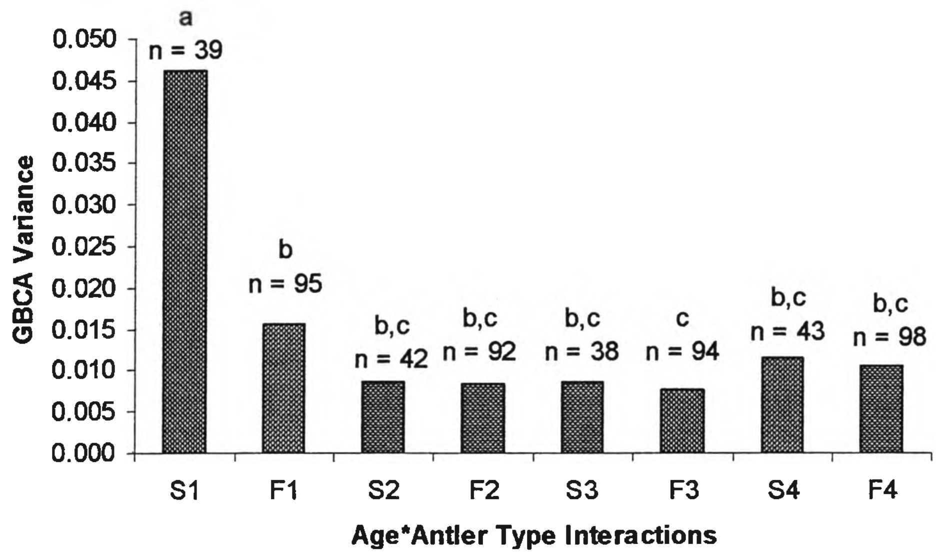

Figure 5. Variance in asymmetries for spike and fork-antlered white-tailed deer bucks for gross Boone and Crockett score asymmetry (GBCA) variances by age groups 1, 2, 3, and 4-years of age. Sample size and groupings are displayed.

The variance (s^2 = 0.077) in antler weight asymmetry for 1-year old bucks differed significantly from all other sets of antlers (Figure 6). The variances in the asymmetry of antler weight of 2-year old and 3-year old bucks were similar, as were the variances in the asymmetries of antler weight of 3 and 4-year old bucks, with 4-year old bucks having the smallest asymmetry variance (s^2 = 0.008).

The asymmetry of antler weight of 1-year old SAY bucks had a significantly larger variance (s^2 = 0.205) than all other interaction groups. SAY bucks at ages 2 and 3-year old and FAY at 1-year old had similar variances in asymmetry, as well as SAY bucks at 2 and 3, and 4-year old and FAY at 4-year old. A similar variance occurred in asymmetry of 3 and 4-year old SAY bucks and 2 and 4-year old FAY bucks. Another subgroup was composed of 4-year old SAY bucks and 2-year old and 3-year old FAY bucks. The variance ($s^2 = 0.008$) in asymmetry of antler weight was the smallest for 3-year old FAY bucks.

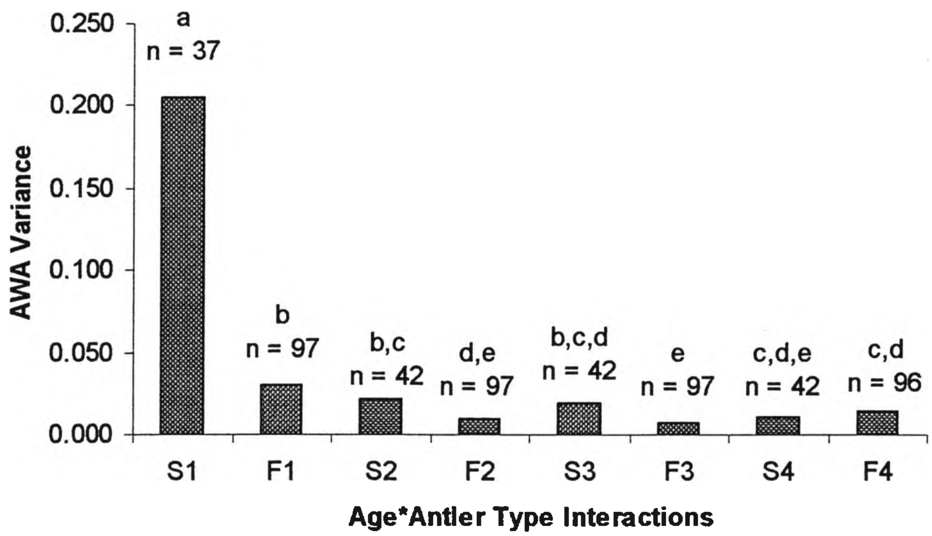

Figure 6. Variance in asymmetries for spike and fork-antlered white-tailed deer bucks for antler weight asymmetry (AWA) variances by age groups 1, 2, 3, and 4-years of age. Sample size and groupings are displayed.

Abnormal Tine Length Asymmetry

The results of Levene's test for homogeneity of variance showed a difference in variance among the abnormal tine length asymmetry based on age, yearling antler type, and the interaction of age and yearling antler type ($p < 0.001$). A difference in variance also occurred separately for age ($p < 0.001$) and yearling antler type ($p < 0.001$).

The antlers of 4-year old FAY bucks had the greatest variance ($s^2 = 1.004$) of all other interaction groups (Figure 7). There were no significant differences in the variance in the asymmetry of antlers of 1-year old FAY bucks and 4-year old SAY bucks. No abnormal tines occurred in the 2-year old and 3-year old age classes for bucks that were FAY or SAY bucks.

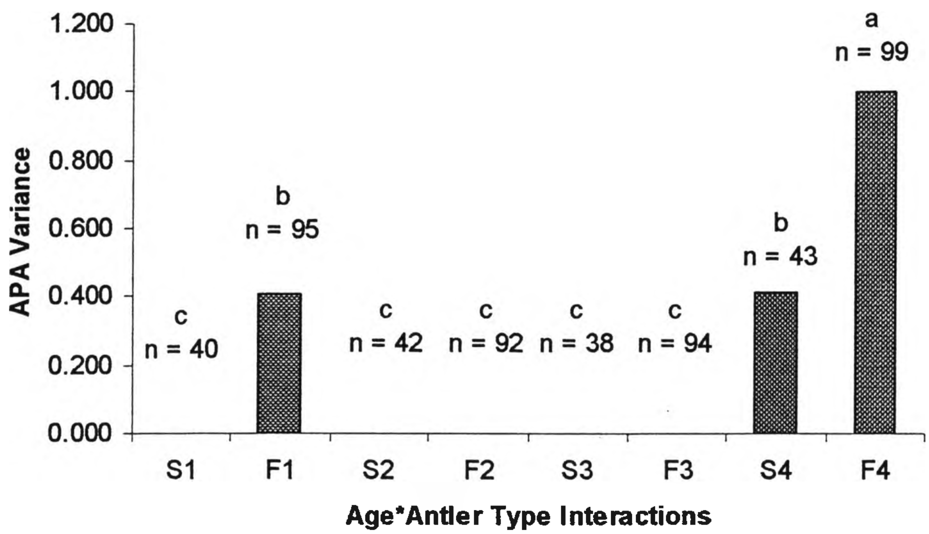

Figure 7. Variance in asymmetries for spike and fork-antlered white-tailed deer bucks for abnormal tine length (APA) variances by age groups 1, 2, 3, and 4-years of age. Sample size and groupings are displayed.

Asymmetry Change with Age

A negative slope was found for all regressions with the exception of the abnormal tine length asymmetry of SAY and FAY bucks. The regression slopes for abnormal tine length for both antler types asymmetry were positive. No regression coefficients differed significantly from 0. All regression coefficients and correlations with the corresponding significance levels are listed in Table 5.

A t-test to evaluate differences in the slopes of asymmetries of antlers for FAY bucks and SAY bucks with relation to age showed no significant differences in the regression slopes for any asymmetry measures (Table 6). The greatest difference in regression slopes of an individual asymmetry was seen in total main beam circumference asymmetry ($0.200 > p > 0.100$). Charts of all asymmetry variances and regression lines are included in appendix B.

Table 5. The results from Linear regression analysis of asymmetry variances based on age for all asymmetry measures of 144 bucks at the Kerr Wildlife Management Area. The regression slope coefficients, intercept coefficient, and significance values are shown.

Trait	Yearling Antler Type	n	Intercept B	p	Slope b	P
MBA	SAY	4	0.0196	0.098	-0.0048	0.185
	FAY	4	0.1590	0.124	-0.0045	0.182
TGA	SAY	3	0.7300	0.138	-0.1910	0.227
	FAY	4	0.2750	0.175	-0.0244	0.552
TTA	SAY	3	0.6240	0.242	-0.1630	0.206
	FAY	4	0.2760	0.175	-0.0244	0.551
THA	SAY	4	0.0129	0.061	-0.0025	0.175
	FAY	4	0.0360	0.060	-0.0092	0.111
GBCA	SAY	4	0.0448	0.140	-0.0104	0.269
	FAY	4	0.0147	0.077	-0.0016	0.411
AWA	SAY	4	0.0272	0.148	-0.0048	0.381
	FAY	4	0.2100	0.130	-0.0583	0.198
APA	SAY	4	0.0966	0.891	0.1800	0.512
	FAY	4	-0.2060	0.402	0.1240	0.225

Table 6. The results from t-test comparisons of linear regression slopes of asymmetry variances based on age grouped by yearling antler type for all asymmetry measures of 144 bucks at the Kerr Wildlife Management Area. The test statistic, degrees of freedom and significance values are shown.

Trait	t-value	df	P
MBA	1.786	4	0.200 > p > 0.100
TGA	-0.931	3	0.500 > p > 0.200
TTA	-0.960	3	0.500 > p > 0.200
THA	1.875	4	0.200 > p > 0.100
GBCA	1.246	4	0.500 > p > 0.200
AWA	1.726	4	0.200 > p > 0.100
APA	0.235	4	p > 0.500

DISCUSSION

Classic characteristics of relative fluctuating asymmetry were found in this study. Fluctuating asymmetry is a measure of small random differences in the right and left sides of bilateral traits (Merlia and Bjorkland 1995). Van Valen (1962) related these differences to inefficiencies in processes that buffer against various environmental perturbations. Among these perturbations may be included lack of nutrition, parasites, and physical injury (Moller 1997). Additionally, Moller (1997) suggests that fluctuating asymmetry also is controlled by genetic deficiencies in the buffering process.

In this study, all bucks had access to an unlimited food supply. This minimized differences in fluctuating asymmetry due to nutritional differences between individuals. Additionally, all bucks lived in the same enclosure and experienced similar risk of parasite infestation and physical injury. This allowed the assumption to be made that environmental conditions were near equal across all tested subgroups and differences to be attributed primarily to differences within individual bucks within each subgroup.

The variance of all asymmetry measures interacted similarly with both age and yearling antler type, with the exception of abnormal tine length. Because of substantial differences in the asymmetry of abnormal tines, this category is not included in the discussion of other asymmetries but will be discussed later. For age class, 1-year old bucks had a larger variance than all other age classes. This result fits the assumption that asymmetry is affected by environmental conditions and a buck's ability to cope with these environmental conditions. Moller (1996) found that in barn swallows (*Hirundo* *rustica*), the greatest asymmetry in wing bars corresponded to the age of most rapid growth. Pelabon and Van Breukelan (1998) reported that roe deer had a greater sensitivity to environmental factors at the yearling age class than at any other. Because of the rapid bone and body growth during the first year of a buck's life, there is a greater demand for available resources within the buck. This means that fewer resources can be allocated to development of a secondary reproductive structure such as antlers during periods of rapid growth. Also, there is a likelihood that minerals allocated for antler development must be drawn from the environment more so than in older age classes, when older bucks use minerals from existing bones to aid in production of antlers (Goss 1983). This would lead to the expectation that asymmetry would be greater in the yearling age class.

There was a general trend for SAY bucks to have a greater variance in the asymmetry of antler characteristics compared to FAY bucks in main beam length, antler weight, main beam circumferences and gross Boone and Crockett score, although the differences were not significant in main beam circumference ($p = 0.076$) and gross Boone and Crockett ($p = 0.360$). Variance in the asymmetry of total normal tine length and total tine length actually showed slightly larger values in FAY bucks, however both of these values were highly non-significant. This is likely due to the effects of an absence of tines in the 1-year old age class of SAY bucks and subsequently not being included in the analysis. This is important because the yearling age class had a significantly larger asymmetry variance than all other age classes. The lack of tines in 1-year old SAY bucks probably contributed to the non-significant result in gross Boone and Crockett score asymmetry, since tine length is a major component of gross Boone and Crockett scores.

Also, the slightly non-significant value for variance in the asymmetry of main beam circumferences may be affected by tine placement on the main beam and tine number, which would affect the variance in FAY bucks more than SAY bucks.

The increased variance in asymmetry of these antler characteristics concurs with the hypothesis of this study that SAY bucks are less able to process nutrients available to them and also less able to cope with the environmental conditions than FAY bucks throughout life. Scribner et al. (1989) found a positive relationship in white-tailed deer bucks between levels of heterozygosity and various measures of antler size. This suggests that individuals with higher levels of heterozygosity are either better competitors for resources in a natural environment and utilize the available resources better than individuals with lower levels of heterozygosity. Ott et al. (1998) showed that SAY bucks have lower quality antlers throughout life than FAY bucks. From these two studies, it can be predicted that SAY bucks may be less heterozygous than FAY bucks because deer with larger antlers may be more heterozygous and FAY bucks have larger antlers throughout life than SAY bucks. Additionally, Palmer and Strobeck (1986) suggested that individuals with greater levels of asymmetry exhibit lower levels of heterozygosity. The greater asymmetry in main beam asymmetry and antler weight asymmetry of SAY bucks than FAY bucks found in this study supports the hypothesis that SAY bucks may be less heterozygous than FAY bucks.

In the interaction of age class and yearling antler type, for all asymmetry measures that had 1-year old SAY bucks included, the asymmetry variances of 1-year old age class of SAY bucks were significantly larger than all other interaction subgroups. One-year old FAY bucks consistently had larger variances than the 3 and 4-year old age classes. These results agree with studies showing that younger roe deer bucks were less capable of coping with environmental conditions than older bucks (Pelabon and Van Breukelen 1998). However, it also suggests that in younger age classes, SAY bucks are even less capable of coping with their environment than FAY bucks, further supporting the hypothesis that SAY bucks may be less heterozygous than FAY bucks.

For all asymmetry measures with the exception of abnormal tine asymmetry, SAY bucks had a greater variance in asymmetry for an age class than FAY bucks, although differences in older age classes were not always significant. The only departures from this occurred in antler weight and total main beam circumference for the 4-year old age class. These data suggest that SAY bucks at all age classes are less able to buffer against environmental conditions than FAY bucks. However, this decrease in buffering ability is not as extreme as in the yearling age class. The fact that at the 4-year old age class the difference in variance is not as consistent shows that the process that causes a difference in the variance of asymmetry of antler characteristics may not be as prevalent in older age classes. One explanation for this could come from the fact that by 4-years of age, competition for nutrients used in body and antler growth has ended because body growth has been completed. This allows a greater allocation of resources for antler growth, which would result in a more stable process of antler development.

The results of the linear regression of the variance of asymmetries for all asymmetry measures for both SAY and FAY bucks showed no significant change in asymmetry in antler characteristics of white-tailed deer with age. This does not follow with the hypothesis that in higher age classes, asymmetries of SAY bucks would decrease at a slower rate than FAY bucks. This suggests that the differences in the buffering processes that govern fluctuating asymmetry in white-tailed deer are likely exposed most during times when the demand for available resources is large and these processes are affected equally across antler types rather than SAY bucks being more susceptible to demand for resources. Such a demand for resources would be constant across antler types for an age class, with the greatest demand for resources in younger age classes. Because bucks were offered unlimited food, all bucks in the study had equal opportunity to meet nutritional demands.

As stated above the differences in the variance in the asymmetry for antler characteristics between antler types is not consistent at the 4-year old age class. This could be explained in the context of sexual selection and signaling. Ditchkoff et al. (2001) found that asymmetry in antlers of white-tailed bucks followed the pattern of a sexually selected trait with a negative relationship between trait size and asymmetry. Similar results were seen in roe deer (Pelabon and Van Breukelan 1998) and reindeer (Markusson and Folstad 1997). These studies, however, looked at patterns primarily from the standpoint of antlers as a weapon in intrasexual competition, but the basic pattern for sexually selected traits as weapons is the same as a mate selection signal.

For a trait to be useful in signaling, other individuals must be able to easily evaluate the trait. For the trait to be truly useful as a mate selection trait, the trait also must be tied to some fitness component. Ditchkoff et al. (2001) showed that asymmetry in the antlers of white-tailed deer was lower in bucks with a greater body weights, suggesting that individuals with lower asymmetry are healthier. However, Ditchkoff et al. (2001) did not find this type of relationship within age classes, meaning that the relationship seen may be more indicative of an effect of age than true individual quality.

Also, as shown above, bucks with lower asymmetry may be more heterozygous than bucks with greater asymmetries. This suggests that asymmetry measures that are visibly evaluated may function as reliable signals.

In this study, no asymmetry measures completely fit the predicted pattern for a sexual signal based on the asymmetry as a measure of individual quality within all age class. However, the asymmetries in total normal tine length, total tine length, and antler weight asymmetries do show the pattern of SAY bucks being more asymmetric than FAY bucks in all but one age class. In the asymmetries of total tine length and total normal tine length, Say bucks were seen to be more asymmetric than FAY bucks at all age classes except in the 3-year old age class, where the two groups showed no difference. Antler weight asymmetry showed SAY bucks to be more asymmetric than FAY bucks at all age classes with the exception of the 4-year old age class, where SAY bucks and FAY bucks showed no difference.

The interactions of age and yearling antler type on the asymmetries of antler weight, total normal tine length, and total tine length seen in this study indicate that these asymmetries show a pattern that indicates that they may function in mate selection. A greater variance in these asymmetries is seen in SAY bucks, which are of lesser antler quality and possibly lesser fitness. Asymmetries evaluated along with trait size of antler weight, total tine length, and total normal tine length could make reliable indicators of male quality. However the actual effectiveness of these traits in mate choice is not indicated by this study.

Abnormal tine length asymmetry is quite different from all other asymmetry measures. Most bucks in this study did not exhibit abnormal tines. The bucks that did possess abnormal tines did so only in the first and fourth years and only on one side of the set of antlers. Because of this, the asymmetry measures were little less than a measure of incidence of abnormal tines. The variance in asymmetry of abnormal tine length increased with age, which was different than that seen in other asymmetry measures. This could indicate that abnormal tines are characters that are contrary to symmetric development that arise only when there is an excess of resources over what is needed for both normal antler production and growth and maintenance of the body. Although this is counter to the patterns exhibited by most sexually signaling traits, the presence of abnormal tines could play a role in signaling. Because the greatest incidence in abnormal tines was in FAY bucks, and specifically in the 4-year old age class, these tines could be very useful in quality recognition along with other traits. However, because of the small incidence of abnormal tines in this study, it impossible to draw any definite conclusions.

Differences in asymmetry based solely on antler type support the suggestion that SAY bucks may be less capable of coping with environmental conditions than FAY bucks and are thus less heterozygous. Further examination of asymmetry in antlers of white-tailed deer is needed before any major management recommendations can be made. From this study some possible implications can be predicted. Populations of white-tailed bucks with significantly higher levels of SAY bucks may be less heterozygous than other populations of white-tailed bucks. Using asymmetry values and antler trait size, managers may be better equipped to evaluate herd quality. Increased asymmetry along with a high incidence of SAY bucks or a more easily recorded antler quality measure may indicate that there is a low level of heterozygosity and possibly an overall genetic deficiency in the herd, and as such, management should be directed toward increasing heterozygosity.

From the results of this study, it is also suggested that managers may be able to evaluate herd quality through the use of a combination of both antler size and relative fluctuation asymmetry in older age classes. Herds that have higher levels of asymmetry in the older age classes may have lower levels of heterozygosity, and management should be directed toward increasing the heterozygosity of the deer in the herd for both better antler development and overall health.

A high level of relative fluctuating asymmetry in bucks that produce larger antlers in older age classes also could indicate lower levels of heterozygosity. However this could also indicate nutritional deficiencies in the habitat or other environmental conditions. It is suggested that managers evaluate components of the habitat more closely to ensure that all nutritional requirements are being met. It is also suggested that the deer be evaluated for possible parasitic or microbial infections.

This study illustrated the relationship between age and the antler type a buck has as a yearling. Age of a deer, especially at the 1-year old age class, was seen to play a large role in the asymmetry of all antler traits measured than any other factor. Since the bucks used in this study lived under conditions of similar nutritional availability, differences in the processing of resources may have been overcome through reduced nutritional stress, especially in the older age classes where there are fewer demands for resources for body growth. In a natural environment, nutritional limitation may become a compounding factor and cause an increased effect. It can be further hypothesized that had the bucks in the older age classes been exposed to equal but limited nutrients, that the differences between SAY bucks and FAY bucks may have been even more dramatic.

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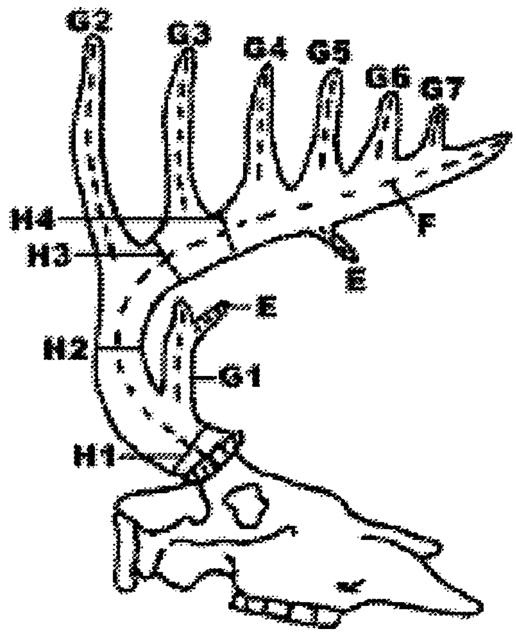
APPENDIX A.

Boone and Crockett Measurements

For White-tailed Deer



A-1 – Measurements for Boone and Crockett Scoring (Boone and Crockett 1999).

F = Main Beam Length

Gi = Normal Tine Lengths

E = Abnormal Tine Lengths

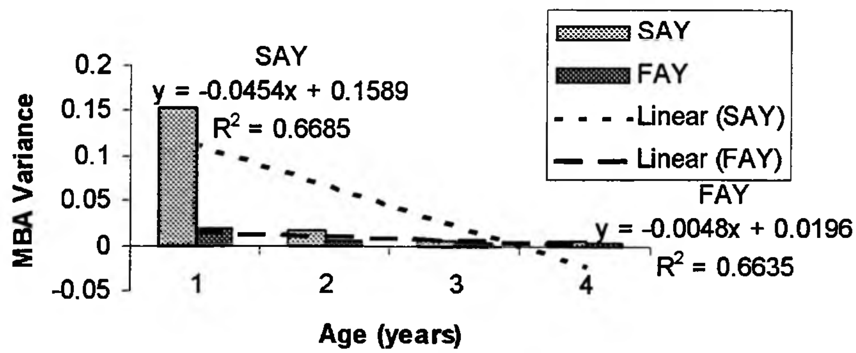
Hi = Main Beam Circumferences

APPENDIX B

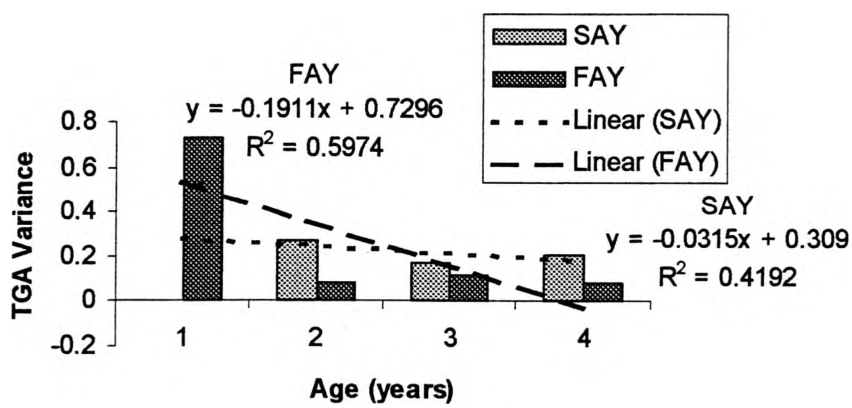
Graphs of Asymmetry Variances vs. Age

with

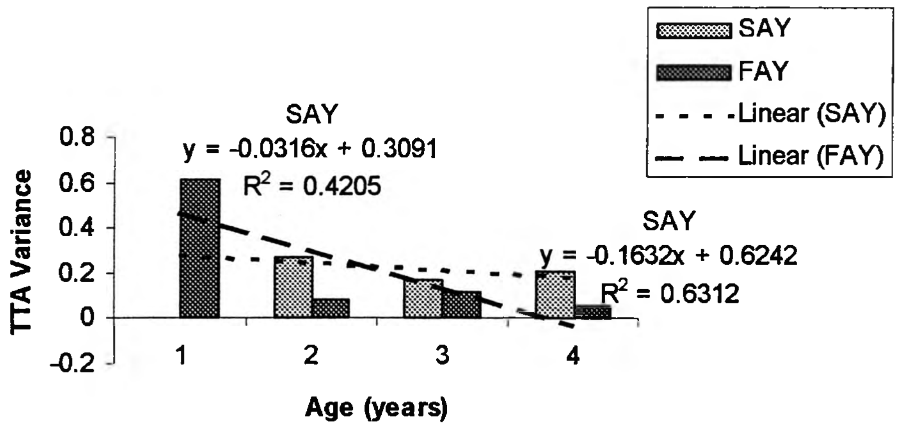
Regression Lines



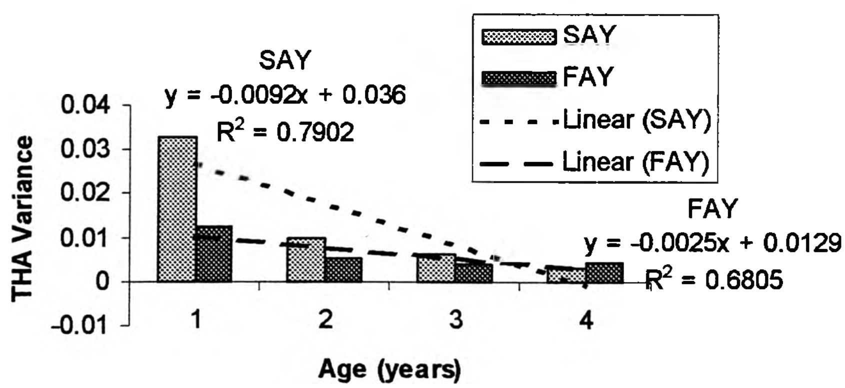
B-1 – Regression lines and equations of variances of main beam length asymmetry vs. deer age for SAY and FAY bucks.



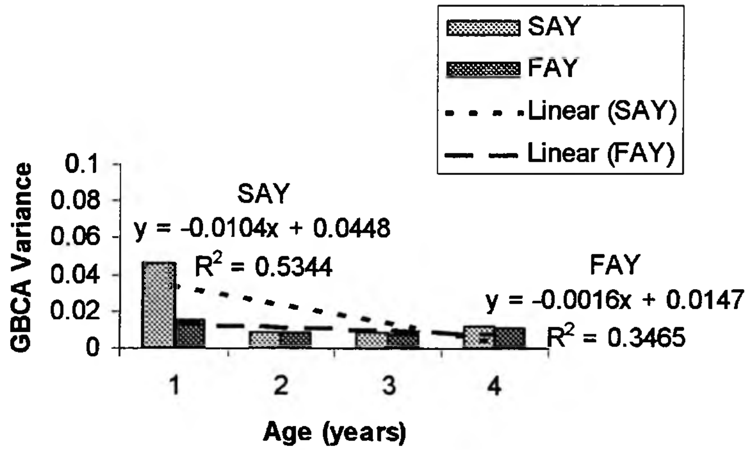
B-2 – Regression lines and equations of variances of total normal tine length asymmetry vs. deer age for SAY and FAY bucks.



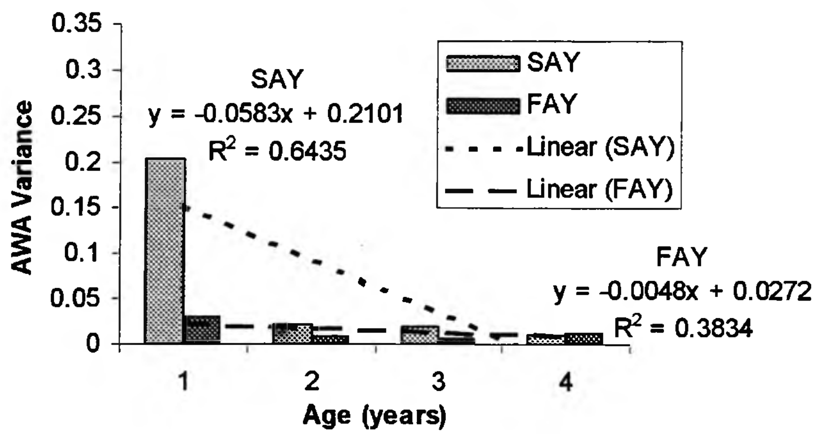
B-3 – Regression lines and equations of variances of total tine length asymmetry vs. deer age for SAY and FAY bucks.



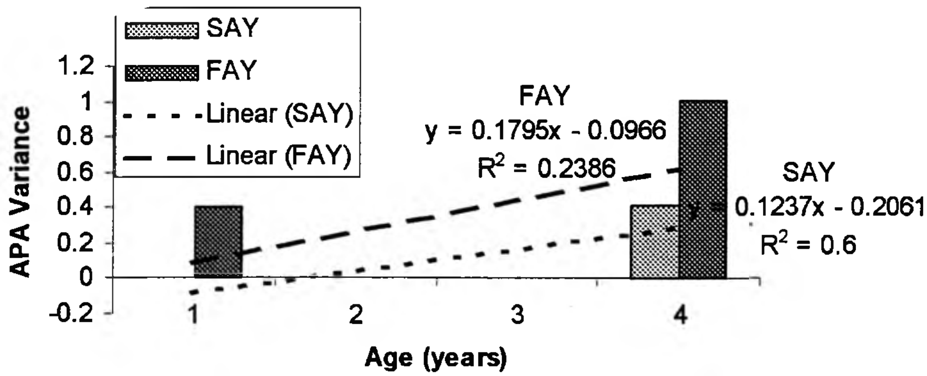
B-4 – Regression lines and equations of variances of main beam circumference asymmetry vs. deer age for SAY and FAY bucks.



B-5 – Regression lines and equations of variances of gross Boone and Crockett score symmetry vs. deer age for SAY and FAY bucks.



B-6 – Regression lines and equations of variances of antler weight asymmetry vs. deer age for SAY and FAY bucks.



B-7 – Regression lines and equations of variances of abnormal point length asymmetry vs. deer age for SAY and FAY bucks.

APPENDIX C.

Gross Boone and Crockett

Component Measurements

Appendix C -- Gross Boone and Crockett score components for 144 male white-tailed deer at the Kerr Wildlife Management Area. Deer Identification number (PID), points (PTS), spread (SPD), left main beam length (MBL), right main beam length (MBR), lengths of left normal tines (LGi), length of right normal tines (RGi), left main beam circumferences (LHi), right main beam circumferences (RHi), number of abnormal points on left side (LAP), number of abnormal points on the right side (RAP), length of all abnormal points on the left side (LAL), length of all abnormal points on the right side (RAL), gross Boone and Crockett score in millimeters (BCSM), gross Boone and Crockett score in inches, left antler weight (AWL), tight antler weight (AWR), deer age (AGE), and number points as a yearling (YPT) are shown.

PID	PTS	SPD	MBL	MBR	LG1	RG1	LG2	RG2	LG3	RG3	LG4	RG4	LG5	RG5	LH1	RH1	LH2	RH2	LH3	RH3	LH4	RH4	LAP	RAP	LAL	RAL	BCSM	BCSI	AWL	AWR	SET	YPT
100016	8	210	296	283	46	31	89	95	54	32	0	0	0	0	68	70	63	60	64	57	39	38	0	0	0	0	1595	62 8	118	114	1	8
100016	8	323	376	373	47	30	143	159	96	116	0	0	0	0	76	79	71	71	76	68	48	42	0	0	0	0	2194	86 4	228	229	2	8
100016	9	350	446	436	60	57	203	232	194	202	67	0	0	0	92	92	79	82	80	76	67	51	0	0	0	0	2866	112.8	361	371	3	8
100016	9	330	375	368	83	70	159	168	140	130	67	0	0	0	89	89	79	76	76	73	64	54	0	0	0	0	2489	98	268	253	4	8
100017	2		.	.	.	.	.	.	.	.	.	.	.	.	.	.		.	.	.	.	.	.	.	.	.	.	.	.		1	2
100017	5	396	260	316	25	0	58	83	0	0	0	0	0	0	64	56	58	56	44	45	44	45	0	0	0	0	1550	61	95	110	2	2
100017	8	510	413	411	41	46	166	163	115	145	0	0	0	0	84	82	79	72	77	68	62	50	0	0	0	0	2584	101.7	326	275	3	2
100017	8	479	381	397	67	32	114	137	60	117	0	0	0	0	86	83	76	73	73	67	60	51	0	0	0	0	2352	93	271	227	4	2
100040	2		158	90	0	0	0	0	0	0	0	0	0	0	40	56	40	51	40	32	40	32	0	0	0	0	0	0	32	26	1	2
100040	6	327	347	280	53	49	37	96	0	0	0	0	0	0	72	73	63	62	51	60	51	60	0	0	0	0	1681	66.2	166	169	2	2
100040	7	360	386	394	60	47	124	139	0	39	0	0	0	0	83	81	73	75	62	70	62	45	0	0	0	0	2100	82.7	270	291	3	2
100040	8	394	438	422	79	54	133	146	95	79	0	0	0	0	98	98	86	83	83	79	60	60	0	0	0	0	2489	98	371	393	4	2
107007	6	.	234	228	35	27	70	49	0	0	0	0	0	0	59	55	51	50	42	39	42	39	0	0	0	0	0	0	227	323	1	6
107007	8	327	320	371	84	76	141	161	106	118	0	0	0	0	83	72	69	67	68	65	52	46	0	0	0	0	2226	87.6	343	415	2	6
107007	7	.	410	358	74	0	185	175	121	0	0	0	0	0	80	78	73	78	68	57	50	57	0	1	0	0	0	0	79	67	3	6
107007	6	311	384	438	0	73	213	197	0	171	0	0	0	0	89	83	89	79	60	83	60	60	0	0	0	0	2390	94	186	190	4	6
173004	4	.	228	237	47	0	0	28	0	0	0	0	0	0	59	46	59	46	41	34	41	34	0	0	0	0	0	0	51	53	1	4
173004	8	431	413	417	84	62	171	65	87	50	0	0	0	0	93	80	70	68	60	60	40	39	0	0	0	0	2290	90 2	272	262	2	4
173004	8	444	506	494	91	94	234	250	159	130	0	0	0	0	105	103	90	88	86	81	51	51	0	0	0	0	3057	120.4	563	552	3	4
173004	10	455	545	560	127	140	276	289	178	197	0	0	0	0	108	117	95	98	95	95	73	73	0	0	54	0	3576	141	708	786	4	4
173005	.		.	.	.		.	.		.	.		.		.	.	.			.	.	.	.	.	.	.	.	.	.	.	1	3
173005	8	427	511	500	118	0	239	175	150	153	0	0	0	0	90	85	90	93	90	110	64	65	1	0	0	0	2961	116.6	488	561	2	3
173005	.	.	590	554	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	953	889	3	3
173005	10	464	610	620	194	165	267	292	229	229	0	32	0	0	111	111	98	98	121	114	89	89	0	0	29	0	3961	156	941	923	4	3
173007	4		226	256	0	0	54	77	0	0	0	0	0	0	52	59	52	59	42	42	42	42	0	0	0	0	0	0	75	88	1	4
173007	8		440	410	50	25	126	132	115	113	0	0	0	0	97	95	73	79	66	69	50	51	0	0	0	0	0	0	.	.	2	4
173007	5	.		.	.			.			.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	3	4
173007	6	408	480	495	0	76	0	197	0	117	0	0	0	0	92	108	79	95	79	89	48	54	0	0	184	0	2602	102	.	.	4	4
173009	2	.	78	86	0	0	0	0	0	0	0	0	0	0	36	40	36	40	36	40	36	40	0	0	0	0	0	0	17	13	1	2
173009	6	263	334	358	33	35	166	154	0	0	0	0	0	0	73	72	64	69	48	52	48	52	0	0	0	0	1821	71.7	188	186	2	2

PID	PTS	SPD	MBL	MBR	LG1	RG1	LG2	RG2	LG3	RG3	LG4	RG4	LG5	RG5	LH1	RH1	LH2	RH2	LH3	RH3	LH4	RH4	LAP	RAP	LAL	RAL	BCSM	BCSI	AWL	AWR	SET	YPT
173009	7	355	353	321	0	30	107	170	41	29	0	0	0	0	80	80	72	75	67	60	50	36	0	0	0	0	1926	75 8	221	231	3	2
173009	8	395	430	460	48	64	146	216	152	130	0	0	0	0	89	92	79	83	79	73	60	54	0	0	0	0	2650	104	361	371	4	2
173023	2	.	106	97	0	0	0	0	0	0	0	0	0	0	37	35	37	35	37	35	37	35	0	0	0	0	0	0	16	13	1	2
173023	8	328	394	388	103	73	172	80	119	112	0	0	0	0	82	76	75	75	72	70	49	50	0	0	0	0	2318	91.3	279	254	2	2
173023	8	356	431	420	112	87	173	193	129	126	0	0	0	0	90	87	87	84	84	74	64	57	0	0	0	0	2654	104 5	370	363	3	2
173023	8	366	475	493	133	121	225	229	175	184	0	0	0	0	92	89	92	92	89	95	67	68	0	0	0	0	3085	121	515	523	4	2
173034	4	.	111	160	.	.	.	.	.	.		.	.	.		.	.	.	.	.	.	.	.	.	.	.	.	.	31	35	1	4
173034	7	.	277	283		.		.	.	.	.	.		.	.	.	.	.	.	.		.	.	.	.	.	.	.	186	184	2	4
173034	7	355	376	380	80	70	143	163	99	0	0	0	0	0	85	83	89	80	74	71	53	46	0	0	0	0	2247	88 5	289	281	3	4
173034	9	351	440	460	51	79	178	165	140	127	25	0	0	0	92	95	89	89	86	89	73	76	0	0	0	0	2705	107	395	403	4	4
173041	2	.	145	140	0	0	0	0	0	0	0	0	0	0	45	49	45	49	45	49	45	49	0	0	0	0	0	0	33	41	1	2
173041	4	278	240	242	0	0	42	37	0	0	0	0	0	0	61	60	61	60	35	35	35	35	0	0	0	0	1221	48.1	120	122	2	2
173041	4	325	259	263	0	0	61	70	0	0	0	0	0	0	61	62	61	62	42	40	42	40	0	0	0	0	1388	54 6	113	109	3	2
173041	3	341	330	340	95	0	0	0	0	0	0	0	0	0	70	67	70	67	48	67	48	67	0	0	0	0	1608	63	194	180	4	2
173046	2	.	21	62	0	0	0	0	0	0	0	0	0	0	10	25	10	25	10	25	10	25	0	0	0	0	0	0	1	6	1	2
173046	6	301	314	323	0	0	107	42	32	83	0	0	0	0	57	63	50	59	38	44	38	44	0	0	0	0	1595	62.8	256	261	2	2
173046	8	385	400	395	66	85	161	156	130	139	0	0	0	0	79	80	70	69	64	65	46	51	0	0	0	0	2441	96 1	264	268	3	2
173046	9	438	456	460	89	98	168	184	143	121	0	0	0	0	83	86	76	76	70	76	54	57	0	0	44	0	2780	109	344	354	4	2
173068	2	.	69	151	0	0	0	0	0	0	0	0	0	0	33	38	33	38	33	38	33	38	0	0	0	0	0	0	24	7	1	2
173068	5	279	291	298	0	30	67	55	0	0	0	0	0	0	58	60	58	60	52	56	52	37	0	0	0	0	1453	57.2	109	114	2	2
173068	9	390	390	404	52	46	147	130	104	125	0	26	0	0	80	80	76	76	74	81	45	62	0	0	0	0	2388	94	242	257	3	2
173068	9	373	445	460	64	64	178	133	146	140	0	25	0	0	86	83	83	83	86	92	51	60	0	0	0	0	2650	104	337	336	4	2
173069	2	.	43	40	0	0	0	0	0	0	0	0	0	0	30	21	30	21	30	21	30	21	0	0	0	0	0	0	4	5	1	2
173069	4	261	268	263	0	0	116	99	0	0	0	0	0	0	60	59	60	59	45	40	45	40	0	0	0	0	1415	55.7	114	111	2	2
173069		.	302	315	.	.	.	.	.	.	.	.		.	.	.	.	.	.	.	.	.	.	.	.	.		.	192	191	3	2
173069	6	300	325	340	149	175	102	98	0	0	0	0	0	0	76	73	70	70	51	41	51	41	0	0	0	0	1962	77	261	263	4	2
173091		.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	1	2
173091		.	.	.	.	.		.		.	.	.	.	.	.	.	.	.	.	.	.		.	.	.	.	.	.	.	.	2	2
173091		.	.	.	.	.	.	.		.		.	.	.	.			.	.	.	.	.	.	.		.	.	.	.	.	3	2
173091	8	337	435	448	95	89	137	146	105	86	0	0	0	0	95	92	89	86	95	92	64	64	0	0	0	0	2554	101	.	.	4	2
174038	3	251	271	188	0	0	72	0	0	0	0	0	0	0	72	68	59	52	52	50	52	50	0	0	0	0	1237	48 7	119	84	1	6
174038	8	.	315	319	.	.		.	.	.	.	.	.		.	.	.	.	.	.	.	.	.	.	.	.	.	.	177	175	2	6
174038	8	356	407	400	0	74	168	126	105	105	0	0	0	0	88	85	75	75	74	90	62	65	0	1	0	0	2356	92.8	312	308	3	6
174038	7	312	314	312	86	51	79	0	0	25	0	0	0	0	73	76	70	70	60	70	60	51	0	0	0	0	1710	67	108	111	4	6
174051	2	328	204	228	0	0	0	0	0	0	0	0	0	0	51	50	51	50	51	50	51	50	0	0	0	0	1164	45 8	60	70	1	2
174051	7	387	378	406	0	25	106	102	101	93	0	0	0	0	72	70	70	69	53	67	53	51	0	0	0	0	2103	82.8	227	220	2	2
174051	8	390	445	440	0	41	151	180	137	153	0	0	0	0	80	85	78	84	76	92	49	72	1	0	0	0	2554	100.6	402	399	3	2
174051	10	445	490	500	41	57	171	143	165	133	0	0	0	0	86	89	83	86	79	89	57	70	0	0	200	0	2984	117	386	456	4	2
174053	4	.	179	206	0	0	0	43	0	0	0	0	0	0	72	66	59	66	42	48	42	48	1	0	43	0	0	0	101	57	1	4
174053	7	411	349	354	77	75	59	117	0	55	0	0	0	0	57	92	74	73	78	66	50	40	0	0	0	0	2027	79.8	214	246	2	4
174053	7	423	391	428	101	87	126	116	0	79	0	0	0	0	101	104	79	83	62	74	37	53	0	0	0	0	2344	92.3	291	332	3	4

PID	PTS	SPD	MBL	MBR	LG1	RG1	LG2	RG2	LG3	RG3	LG4	RG4	LG5	RG5	LH1	RH1	LH2	RH2	LH3	RH3	LH4	RH4	LAP	RAP	LAL	RAL	BCSM	BCSI	AWL	AWR	SET	YPT
174053	9	408	423	450	76	89	98	121	73	89	0	0	0	0	102	98	83	86	86	83	64	67	0	0	29	0	2522	99	347	372	4	4
174061	5	165	174	218	52	75	37	0	0	0	0	0	0	0	62	63	55	63	30	51	30	51	0	0	0	0	1126	44 3	64	81	1	5
174061		.	363	443		.	.	.	.	.		.		.	.	.	.	.	.	.	.	.	.	.	.			.	281	310	2	5
174061	7	290	361	432	0	40	135	138	97	118	0	0	0	0	95	93	89	85	82	84	61	64	0	0	0	0	2264	89.1	370	390	3	5
174061	8	330	425	433	54	60	124	137	0	38	0	0	0	0	95	95	89	89	76	76	41	54	0	0	0	0	2217	87	339	354	4	5
174093	4	341	292	275	0	0	78	61	0	0	0	0	0	0	60	60	45	60	30	45	30	45	0	0	0	0	1422	56	107	113	1	4
174093	8	389	423	440	52	43	113	129	134	146	0	0	0	0	88	86	75	74	71	72	53	51	0	0	0	0	2439	96	276	292	2	4
174093	9	390	465	438	50	58	134	167	175	174	125	0	0	0	103	101	89	92	93	79	74	57	0	0	0	0	2864	112.8	456	426	3	4
174093	10	445	487	490	48	57	140	114	197	203	162	206	0	0	111	117	95	98	105	149	83	83	0	0	0	0	3391	133	523	536	4	4
174094	6	236	279	263	30	41	33	84	0	0	0	0	0	0	65	70	54	61	34	39	34	39	0	0	0	0	1362	53.6	89	96	1	6
174094			351	340		.		.	.	.	.	.	.	.		.	.	.	.	.		.	.	.	.	.	.	.	155	173	2	6
174094	8	357	416	420	101	69	130	228	116	80	0	0	0	0	90	87	77	80	72	74	47	50	0	0	0	0	2494	98 2	332	349	3	6
174094	8	381	414	403	64	73	168	149	105	48	0	0	0	0	89	89	79	79	70	73	54	51	0	0	0	0	2389	94	346	328	4	6
174192	5	240	202	208	39	0	94	115	0	0	0	0	0	0	65	55	54	55	45	45	38	45	0	0	0	0	1300	51.2	74	76	1	5
174192	6	344	321	297	33	0	145	167	101	0	0	0	0	0	69	69	61	64	59	55	42	55	0	0	0	0	1882	74.1	162	151	2	5
174192	10	374	464	465	73	70	250	215	221	252	0	128	0	30	95	98	94	82	85	88	53	68	0	0	0	0	3205	126.18	347	295	3	5
174192	8	368	444	502	73	73	273	260	200	232	0	0	0	0	92	95	83	83	76	83	51	60	0	0	0	0	3048	120	340	403	4	5
175064	2	133	169	135	0	0	0	0	0	0	0	0	0	0	36	36	36	36	36	36	36	36	0	0	0	0	725	28.5	26	20	1	2
175064	4	247	331	312	0	0	111	106	0	0	0	0	0	0	61	59	61	59	49	44	49	44	0	0	0	0	1533	60 4	137	190	2	2
175064		.	380	380	.	.	.	.		.		.	.	.	.	.	.	.	.	.	.	.		.		.	.		190	179	3	2
175064	7	297	351	330	25	60	133	86	29	0	0	0	0	0	67	64	60	57	54	54	35	35	0	0	0	0	1737	68	149	125	4	2
176046	2	170	145	159	0	0	0	0	0	0	0	0	0	0	36	39	36	39	36	39	36	39	0	0	0	0	774	30.5	22	25	1	2
176046	8	244	277	307	51	61	62	87	42	77	0	0	0	0	59	63	55	57	53	57	32	37	0	0	0	0	1621	63.8	92	115	2	2
176046	8	267	380	375	62	77	104	168	117	134	0	0	0	0	68	68	64	70	72	69	59	43	0	0	0	0	2197	86.5	180	206	3	2
176046	8	269	339	329	89	95	152	194	156	152	0	0	0	0	73	73	73	76	76	76	60	48	0	0	0	0	2331	92	237	243	4	2
177005	5	255	305	321	36	0	130	92	0	0	0	0	0	0	71	68	59	59	52	46	32	46	0	0	0	0	1572	61.9	140	129	1	5
177005	7	416	454	456	0	60	135	196	109	153	0	0	0	0	75	83	75	77	52	74	52	51	0	0	0	0	2518	99.1	360	315	2	5
177005	9	502	499	520	99	91	216	133	161	141	0	40	0	0	90	96	81	80	81	80	61	63	0	0	0	0	3034	119.4	466	460	3	5
177005	8	489	555	585	102	76	232	178	197	187	0	0	0	0	95	102	86	83	89	89	67	73	0	0	0	0	3283	129	602	578	4	5
177009	6	272	278	281	47	0	77	34	0	29	0	0	0	0	60	61	53	59	40	52	40	31	0	0	0	0	1414	55.7	101	99	1	6
177009	8	399	420	425	107	96	136	164	84	63	0	0	0	0	75	75	67	76	63	65	42	44	0	0	0	0	2401	94.5	268	254	2	6
177009	9	490	473	500	125	115	191	195	164	148	56	0	0	0	89	89	80	79	81	76	70	57	0	0	0	0	3078	121.2	411	400	3	6
177009	8	490	563	540	156	168	206	200	137	114	0	0	0	0	92	89	83	83	83	79	67	57	0	0	0	0	3206	126	501	459	4	6
177014	7	245	348	328	56	54	106	110	59	0	0	0	0	0	72	72	65	63	57	54	40	37	0	0	0	0	1766	69.5	185	167	1	7
177014	8	377	447	484	80	80	232	215	130	166	0	0	0	0	90	90	79	82	76	81	50	61	0	0	0	0	2820	111	423	439	2	7
177014	10	412	486	515	101	99	245	217	168	187	0	40	0	0	105	100	92	90	90	92	64	79	1	0	0	0	3183	125.3	648	622	3	7
177014	9	430	515	548	114	111	273	295	130	184	0	0	0	0	105	105	95	95	95	95	79	70	0	0	25	0	3366	133	733	749	4	7
177021	5	166	228	215	0	0	31	53	0	32	0	0	0	0	46	54	46	54	26	51	26	31	0	0	0	0	1059	41.7	49	51	1	5
177021	7	241	362	346	77	0	112	135	105	101	0	0	0	0	66	65	62	63	64	48	43	29	0	0	0	0	1919	75.6	171	170	2	5
177021	8	301	377	396	99	84	165	152	140	155	0	0	0	0	76	76	67	70	71	71	49	53	0	0	0	0	2402	94.6	235	264	3	5
177021	11	294	455	421	121	124	181	219	171	194	79	41	0	0	86	89	79	79	86	86	76	67	0	0	0	0	2948	116	369	363	4	5

PID	PTS	SPD	MBL	MBR	LG1	RG1	LG2	RG2	LG3	RG3	LG4	RG4	LG5	RG5	LH1	RH1	LH2	RH2	LH3	RH3	LH4	RH4	LAP	RAP	LAL	RAL	BCSM	BCSI	AWL	AWR	SET	YPT
177023	4	233	253	242	0	0	114	129	0	0	0	0	0	0	64	62	60	62	49	45	49	45	0	0	0	0	1407	55.4	101	100	1	4
177023	8	307	376	368	29	68	173	186	123	147	0	0	0	0	74	81	68	73	65	69	48	55	0	0	0	0	2310	90 9	247	279	2	4
177023	9	356	403	422	0	56	191	180	190	193	103	74	0	0	85	90	79	81	75	79	70	70	0	0	0	0	2797	110.1	403	437	3	4
177023	12	319	506	465	89	60	260	178	191	229	44	130	108	0	102	114	89	92	83	89	86	86	0	0	25	0	3344	132	607	600	4	4
177025	2	110	95	62	0	0	0	0	0	0	0	0	0	0	34	35	34	35	34	35	34	35	0	0	0	0	543	21.4	9	14	1	2
177025	2	208	184	181	0	0	0	0	0	0	0	0	0	0	49	50	49	50	49	50	49	50	0	0	0	0	969	38.1	47	53	2	2
177025	2	243	215	224	0	0	0	0	0	0	0	0	0	0	57	54	57	54	57	54	57	54	0	0	0	0	1126	44.3	84	88	3	2
177025	2	279	239	257	0	0	0	0	0	0	0	0	0	0	57	64	57	64	57	64	57	64	0	0	0	0	1258	50	90	103	4	2
177033	4	210	220	221	26	0	30	0	0	0	0	0	0	0	55	59	44	47	31	53	31	31	0	0	0	0	1058	41.7	56	54	1	4
177033	10	314	376	386	38	37	86	84	125	126	38	85	0	0	70	70	67	69	94	93	50	62	0	0	0	0	2270	89.4	196	225	2	4
177033	8	377	441	442	87	75	170	168	111	151	0	0	0	0	90	86	86	88	94	97	53	66	0	0	0	0	2682	105.6	395	413	3	4
177033	10	408	545	525	114	102	213	191	206	194	60	92	0	0	102	95	95	95	108	117	73	89	0	0	0	0	3424	135	601	579	4	4
177034	4	228	176	187	0	0	62	43	0	0	0	0	0	0	52	57	52	46	36	28	36	28	0	0	0	0	1031	40.6	51	56	1	4
177034	4	229	236	210	42	94	0	0	0	0	0	0	0	0	72	78	72	78	44	45	44	45	0	0	0	0	1289	50.7	71	70	2	4
177034	8	355	328	319	63	62	136	109	80	94	0	0	0	0	79	81	61	61	52	54	35	38	0	0	0	0	2007	79	173	163	3	4
177034	9	345	400	377	73	76	168	191	171	121	64	0	0	0	92	92	76	73	70	64	64	48	0	0	0	0	2563	101	298	258	4	4
177037	2	.	9	10			.	.	.	.	.	.		.	.	.	.	.	.	.	.	.	.	.		.	.	.	.	.	1	2
177037	2	.	70	78	0	0	0	0	0	0	0	0	0	0	51	36	51	36	51	36	51	36	0	0	0	0	0	0	10	11	2	2
177037	4	334	234	331	26	0	0	69	0	0	0	0	0	0	60	67	60	61	48	48	48	48	0	0	0	0	1264	49.8	74	125	3	2
177037	5	310	285	367	38	0	76	111	0	0	0	0	0	0	67	70	60	70	51	60	51	60	0	0	0	0	1676	66	105	155	4	2
177043	2	76	43	32	0	0	0	0	0	0	0	0	0	0	30	25	30	25	30	25	30	25	0	0	0	0	371	14 6	4	3	1	2
177043	3	228	191	213	0	0	28	0	0	0	0	0	0	0	54	56	54	56	36	56	36	56	0	0	0	0	1064	41 9	67	77	2	2
177043	4	261	255	241	0	0	72	71	0	0	0	0	0	0	67	66	67	66	57	41	57	41	0	0	0	0	1362	53.6	130	127	3	2
177043	4	302	312	336	0	0	86	95	0	0	0	0	0	0	76	76	76	76	57	60	57	60	0	0	0	0	1671	66	195	208	4	2
177046	5	211	229	225	0	41	68	44	0	0	0	0	0	0	65	83	65	64	45	45	45	45	0	0	0	0	1275	50.2	95	92	1	5
177046	8	322	333	335	37	42	164	153	34	98	0	0	0	0	83	78	76	72	63	69	35	50	0	0	0	0	2044	80.5	251	247	2	5
177046	8	360	375	373	42	50	170	187	101	104	0	0	0	0	85	92	82	82	75	75	52	46	0	0	0	0	2351	92.6	330	351	3	5
177046	8	360	441	437	57	60	184	210	162	140	0	0	0	0	89	92	89	89	86	83	64	64	0	0	0	0	2705	106	469	487	4	5
177047	.	.	217	215	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	57	60	1	4
177047	.	.	340	332	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	206	207	2	4
177047	8	348	433	404	64	25	123	203	189	171	0	0	0	0	82	82	72	72	69	66	44	41	0	0	0	0	2488	98	322	322	3	4
177047	8	380	482	458	57	57	149	171	197	203	0	0	0	0	95	98	76	76	73	73	51	54	0	0	0	0	2752	108	379	377	4	4
178001	7	236	336	321	46	76	104	97	58	0	0	0	0	0	73	91	64	62	59	51	40	51	0	0	0	0	1765	69 5	174	190	1	7
178001	8	366	375	440	107	100	124	197	46	125	0	0	0	0	93	91	79	77	73	72	62	51	0	0	0	0	2478	97.6	301	371	2	7
178001	10	403	379	429	119	120	132	126	69	144	0	0	0	0	96	100	79	84	74	78	52	50	1	1	0	0	2536	99.8	392	322	3	7
178001	12	480	539	546	140	127	260	232	194	203	0	0	0	0	108	105	95	92	89	92	73	73	0	0	216	0	3664	144	674	673	4	7
178019	2	178	215	185	0	0	0	0	0	0	0	0	0	0	57	54	57	54	57	54	57	54	0	0	0	0	1022	40.2	58	74	1	2
178019	6	282	268	266	29	34	115	87	0	0	0	0	0	0	76	79	73	69	49	50	49	50	0	0	0	0	1576	62	159	148	2	2
178019	6	298	335	324	73	0	139	157	71	0	0	0	0	0	90	95	89	95	74	76	51	76	0	0	0	0	2043	80.4	326	281	3	2
178019	7	393	381	393	86	89	178	140	0	0	0	0	0	0	98	98	95	89	60	64	60	64	0	0	29	0	2316	91	396	362	4	2
178020		.	340	310	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.		.	.	123	130	1	6

PID	PTS	SPD	MBL	MBR	LG1	RG1	LG2	RG2	LG3	RG3	LG4	RG4	LG5	RG5	LH1	RH1	LH2	RH2	LH3	RH3	LH4	RH4	LAP	RAP	LAL	RAL	BCSM	BCSI	AWL	AWR	SET	YPT
178020	.	.	456	450		.	.	.		.	.	.	.	.	.			.	.	.	.	.	.	.	.	.	.	.	383	344	2	6
178020	.	.	495	505		.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.		.	604	524	3	6
178020	15	450	565	565	162	143	295	267	260	241	121	67	0	0	114	111	102	98	95	98	92	92	0	0	346	0	4285	169	906	756	4	6
178022	4	245	246	251	0	0	49	55	0	0	0	0	0	0	61	55	50	55	40	44	40	33	0	0	0	0	1224	48.2	77	85	1	4
178022	8	308	342	354	33	40	136	129	136	137	0	0	0	0	83	85	68	71	62	61	40	42	0	0	0	0	2127	83.7	220	222	2	4
178022	8	360	420	433	42	53	212	176	181	202	0	0	0	0	98	96	79	80	70	75	46	53	0	0	0	0	2676	105.4	350	372	3	4
178022	10	403	432	463	54	57	184	197	140	191	146	0	0	0	102	98	83	86	95	79	70	60	0	0	25	0	2965	117	366	380	4	4
178023	2	181	196	205	0	0	0	0	0	0	0	0	0	0	50	45	50	45	50	45	50	45	0	0	0	0	962	37.9	55	54	1	2
178023	4	257	248	239	0	0	57	64	0	0	0	0	0	0	59	57	59	57	36	41	36	41	0	0	0	0	1251	49.3	99	92	2	2
178023	4	290	318	310	0	0	115	114	0	0	0	0	0	0	78	75	76	75	58	56	58	56	0	0	0	0	1679	66.1	208	187	3	2
178023	6	297	345	334	0	25	108	111	0	0	0	0	0	0	83	76	73	73	57	54	57	54	0	0	0	0	1748	69	205	198	4	2
178032	6	220	247	262	51	51	115	69	0	0	0	0	0	0	67	68	60	71	40	39	40	39	0	0	0	0	1439	56.7	90	84	1	6
178032	8	295	406	370	63	49	174	192	140	110	0	0	0	0	75	82	71	73	63	62	45	38	0	0	0	0	2308	90.9	234	226	2	6
178032	10	330	437	412	90	88	202	257	206	207	119	0	0	0	92	92	87	92	81	80	65	54	1	0	0	0	2992	117.8	417	385	3	6
178032	9	321	.	445	232	98	298	324	0	219	0	0	0	0	105	98	105	102	60	86	60	57	0	0	175	0	0	0	434	504	4	6
178034	6	279	301	318	58	58	89	90	0	0	0	0	0	0	78	77	68	68	47	50	47	50	0	0	0	0	1678	66.1	163	165	1	6
178034	8	402	423	428	99	92	162	155	44	58	0	0	0	0	94	90	78	81	66	64	47	44	0	0	0	0	2427	95.6	322	327	2	6
178034	8	420	494	495	123	105	214	207	162	126	0	0	0	0	108	106	92	91	80	84	66	57	0	0	0	0	3030	119.3	572	545	3	6
178034	9	410	508	516	127	121	184	241	187	181	41	0	0	0	105	108	95	95	89	92	83	70	0	0	0	0	3253	128	616	625	4	6
178035	8	249	329	320	34	39	109	115	98	102	0	0	0	0	80	85	70	70	61	66	49	47	0	0	0	0	1923	75.7	194	206	1	8
178035	8	308	345	358	64	74	179	164	149	132	0	0	0	0	94	92	76	73	72	71	44	52	0	0	0	0	2347	92.4	299	315	2	8
178035	8	350	433	460	79	97	222	218	195	176	0	0	0	0	113	123	91	90	91	96	65	76	0	0	0	0	2975	117.1	551	566	3	8
178035	17	381	500	500	98	102	241	181	216	197	0	133	0	0	114	111	108	102	98	175	70	98	0	0	117	0	3543	139	699	675	4	8
178038	4	195	145	191	0	26	0	31	0	0	0	0	0	0	46	54	46	47	46	33	46	33	0	0	0	0	939	37	53	40	1	4
178038	7	277	286	283	76	60	71	83	33	0	0	0	0	0	67	71	55	55	42	45	29	23	0	0	0	0	1556	61.3	127	127	2	4
178038	8	326	355	359	129	98	134	130	103	90	0	0	0	0	83	80	69	68	61	61	47	40	0	0	0	0	2233	87.9	265	251	3	4
178038	8	359	396	415	140	111	146	140	83	137	0	0	0	0	89	92	73	76	70	73	54	54	0	0	0	0	2507	99	294	316	4	4
178039	2	147	166	162	0	0	0	0	0	0	0	0	0	0	46	42	46	42	46	42	46	42	0	0	0	0	827	32.6	38	37	1	2
178039	7	294	275	278	35	36	109	112	79	0	0	0	0	0	72	68	65	61	57	38	36	38	0	0	0	0	1653	65.1	118	134	2	2
178039	8	338	375	355	70	60	150	144	110	89	0	0	0	0	89	84	75	75	66	63	40	38	0	0	0	0	2221	87.4	271	259	3	2
178039	8	376	391	395	73	73	203	181	121	133	0	0	0	0	89	86	83	83	70	73	51	51	0	0	0	0	2530	100	330	312	4	2
178041	8	288	318	300	68	70	114	136	44	62	0	0	0	0	76	78	63	69	57	60	44	39	0	0	0	0	1886	74.3	165	173	1	8
178041	8	377	424	398	87	92	177	176	117	109	0	0	0	0	87	86	79	77	68	68	48	46	0	0	0	0	2516	99.1	320	323	2	8
178041	10	425	487	480	102	100	239	253	194	164	81	0	0	0	101	106	91	89	89	80	72	58	0	1	0	0	3212	126 5	571	551	3	8
178041	10	430	527	520	111	111	213	248	194	184	86	25	0	0	108	108	95	95	102	92	79	73	0	0	0	0	3401	134	639	630	4	8
178045	2	170	152	141	0	0	0	0	0	0	0	0	0	0	39	38	39	38	39	38	39	38	0	0	0	0	771	30.4	22	47	1	2
178045	8	353	378	365	45	41	101	115	65	40	0	0	0	0	68	68	65	65	57	54	40	36	0	0	0	0	1956	77	172	161	2	2
178045	8	410	424	451	80	59	162	149	155	143	0	0	0	0	88	86	84	81	78	75	56	56	0	0	0	0	2637	103.8	370	352	3	2
178045	8	442	507	495	83	108	178	184	175	187	0	0	0	0	89	98	89	89	89	89	67	67	0	0	0	0	3035	119	502	494	4	2
178049	2	129	141	173	0	0	0	0	0	0	0	0	0	0	38	41	38	41	38	41	38	41	0	0	0	0	759	29.9	31	21	1	2
178049	6	273	306	312	27	33	97	98	0	0	0	0	0	0	69	70	63	62	44	48	44	48	0	0	0	0	1594	62.8	124	131	2	2

PID	PTS	SPD	MBL	MBR	LG1	RG1	LG2	RG2	LG3	RG3	LG4	RG4	LG5	RG5	LH1	RH1	LH2	RH2	LH3	RH3	LH4	RH4	LAP	RAP	LAL	RAL	BCSM	BCSI	AWL	AWR	SET	YPT
178049	8	340	369	385	65	65	165	152	101	119	0	0	0	0	90	92	80	78	71	75	44	50	0	0	0	0	2341	92.2	279	294	3	2
178049	8	358	423	454	76	83	178	152	133	165	0	0	0	0	102	98	86	89	79	83	54	60	0	0	0	0	2673	105	338	371	4	2
178052	6	305	308	290	62	47	143	0	68	0	0	0	0	0	63	63	56	63	62	52	37	52	0	0	0	0	1671	65.8	150	91	1	6
178052	9	409	399	459	97	90	98	234	40	161	0	27	0	0	85	85	80	80	80	85	60	69	0	0	0	0	2638	103.9	286	401	2	6
178052	9	427	497	510	115	111	302	312	201	219	0	0	0	0	94	96	83	89	94	94	51	69	0	2	0	0	3366	132.5	556	591	3	6
178052	11	452	578	566	124	130	321	305	241	254	175	206	0	0	102	98	98	98	127	127	114	108	0	0	32	0	4257	168	810	829	4	6
178053	6	265	338	298	50	0	93	120	43	0	0	0	0	0	62	61	56	57	62	37	35	37	0	0	0	0	1614	63.5	122	107	1	6
178053	8	382	440	431	76	72	192	212	114	129	0	0	0	0	79	78	72	71	71	69	45	41	0	0	0	0	2574	101.3	285	271	2	6
178053	8	350	499	509	130	104	233	205	156	122	0	0	0	0	89	86	77	79	78	84	50	48	0	0	0	0	2899	114.1	380	412	3	6
178053	8	482	596	594	114	178	273	343	210	130	0	0	0	0	92	95	86	86	98	83	60	51	0	0	0	0	3571	141	530	562	4	6
178063	2	110	70	61	0	0	0	0	0	0	0	0	0	0	37	36	37	36	37	36	37	36	0	0	0	0	533	21	8	11	1	2
178063	4	343	301	279	0	0	85	46	0	0	0	0	0	0	55	52	55	52	32	26	32	26	0	0	0	0	1384	54.5	114	100	2	2
178063	5	383	371	395	0	26	146	75	0	0	0	0	0	0	65	75	65	65	45	52	45	52	0	0	0	0	1860	73.2	203	227	3	2
178063	5	443	425	415	191	67	0	194	0	0	0	0	0	0	73	89	73	70	51	54	51	54	0	0	0	0	2248	89	266	268	4	2
178067	2	98	128	102	0	0	0	0	0	0	0	0	0	0	39	38	39	38	39	38	39	38	0	0	0	0	636	25	21	15	1	2
178067	8	313	390	411	56	72	179	140	97	82	0	0	0	0	69	67	69	62	60	60	40	42	0	0	0	0	2209	87	206	201	2	2
178067	9	314	486	482	143	84	211	214	171	195	0	24	0	0	86	81	81	76	80	80	55	68	0	0	0	0	2931	115.4	382	374	3	2
178067	8	329	546	454	159	105	225	244	178	137	0	0	0	0	89	89	86	86	79	83	60	70	0	0	0	0	3018	119	455	384	4	2
178071	6	190	243	229	63	68	30	31	0	0	0	0	0	0	57	59	49	45	29	27	29	27	0	0	0	0	1176	46.3	74	66	1	6
178071	7	333	384	397	78	79	127	131	0	74	0	0	0	0	75	75	63	63	53	58	53	39	0	0	0	0	2082	82	183	205	2	6
178071	8	375	471	466	119	109	180	196	147	145	0	0	0	0	92	89	81	80	86	82	79	53	0	0	0	0	2850	112 2	418	413	3	6
178071	9	407	510	519	143	137	203	225	194	159	54	0	0	0	98	95	89	92	95	89	70	64	0	0	0	0	3243	128	529	532	4	6
178079	2	147	62	61	0	0	0	0	0	0	0	0	0	0	36	38	36	38	36	38	36	38	0	0	0	0	566	22.3	10	10	1	2
178079	3	340	332	314	0	0	0	70	0	0	0	0	0	0	57	56	57	56	57	37	57	37	0	0	0	0	1470	57.9	117	104	2	2
178079	6	420	410	407	56	48	178	169	0	0	0	0	0	0	83	84	71	70	59	53	59	53	0	0	0	0	2220	87.4	251	236	3	2
178079	6	465	468	469	70	60	235	200	0	0	0	0	0	0	89	89	79	76	57	60	57	60	0	0	0	0	2535	100	317	297	4	2
179006	4	233	227	241	41	0	38	0	0	0	0	0	0	0	63	46	43	46	30	46	30	46	0	0	0	0	1130	44.5	69	62	1	4
179006	8	454	445	455	66	70	224	180	132	79	0	0	0	0	86	90	77	76	72	66	49	42	0	0	0	0	2663	104 8	360	358	2	4
179006	8	408	535	517	89	82	222	245	128	145	0	0	0	0	100	99	88	87	76	84	50	51	0	0	0	0	3006	118.3	552	518	3	4
179006	8	410	533	537	117	117	251	244	140	130	0	0	0	0	108	105	95	92	83	83	51	57	0	0	0	0	3153	124	570	565	4	4
179018	2	119	150	152	0	0	0	0	0	0	0	0	0	0	39	40	39	40	39	40	39	40	0	0	0	0	737	29	87	24	1	2
179018	4	225	340	339	0	0	152	145	0	0	0	0	0	0	66	62	66	62	54	57	54	57	0	0	0	0	1679	66.1	159	155	2	2
179018	8	285	398	414	44	62	209	208	89	41	0	0	0	0	85	85	76	74	70	65	40	38	0	0	0	0	2283	89.9	288	274	3	2
179018	8	292	447	445	83	57	197	197	117	64	0	0	0	0	98	92	83	83	73	73	51	48	0	0	0	0	2498	98	318	295	4	2
179021	2	135	39	88	0	0	0	0	0	0	0	0	0	0	28	32	28	32	28	32	28	32	0	0	0	0	502	19.8	4	11	1	2
179021	4	257	258	273	0	0	65	84	0	0	0	0	0	0	61	67	52	55	41	37	41	37	0	0	0	0	1328	52.3	90	96	2	2
179021	7	355	318	340	24	24	88	111	62	0	0	0	0	0	75	75	60	60	50	45	26	45	0	0	0	0	1758	69.2	172	164	3	2
179021	8	373	379	380	38	32	168	159	130	89	0	0	0	0	86	83	73	70	64	60	44	44	0	0	0	0	2272	89	254	222	4	2
179027	2	212	235	224	0	0	0	0	0	0	0	0	0	0	43	45	43	45	30	32	30	32	0	0	0	0	971	38.2	60	60	1	2
179027	8	280	351	362	51	26	154	160	62	30	0	0	0	0	95	83	75	71	67	64	27	34	0	0	0	0	1992	78.4	250	233	2	2
179027	8	375	450	434	104	79	183	204	30	88	0	0	0	0	105	98	85	81	65	70	35	43	0	0	0	0	2529	99.6	377	378	3	2

PID	PTS	SPD	MBL	MBR	LG1	RG1	LG2	RG2	LG3	RG3	LG4	RG4	LG5	RG5	LH1	RH1	LH2	RH2	LH3	RH3	LH4	RH4	LAP	RAP	LAL	RAL	BCSM	BCSI	AWL	AWR	SET	YPT
179027	8	420	447	470	114	114	181	187	102	83	0	0	0	0	102	102	86	83	76	76	51	51	0	0	0	0	2744	108	409	415	4	2
179028	3	142	94	167	36	0	0	0	0	0	0	0	0	0	65	43	65	43	35	43	35	43	0	0	0	0	811	31.9	36	21	1	3
179028	4	293	354	336	49	0	0	162	0	0	0	0	0	0	84	79	84	70	66	53	66	53	0	0	0	0	1749	68 9	154	188	2	3
179028	6	302	388	378	0	65	0	169	0	82	0	0	0	0	66	81	66	72	66	62	66	40	2	0	0	0	1905	75	180	243	3	3
179028	9	319	345	381	0	73	194	152	0	149	0	0	0	0	79	86	79	76	48	70	48	48	0	0	105	0	2252	89	203	264	4	3
179032	3	.	182	172	0	0	32	0	0	0	0	0	0	0	46	45	46	45	39	45	39	45	0	0	0	0	0	0	.	.	1	3
179032	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	2	3
179032	.	.	455	455	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	623	539	3	3
179032	13	376	497	500	111	111	298	289	216	210	0	0	0	0	102	95	98	98	124	117	76	64	0	0	616	0	3999	157	837	714	4	3
179035	2	212	204	205	0	0	0	0	0	0	0	0	0	0	49	50	49	50	49	50	49	50	0	0	0	0	1017	40	61	64	1	2
179035	4	293	306	300	0	0	105	102	0	0	0	0	0	0	64	65	64	65	51	50	51	50	0	0	0	0	1566	61.7	152	153	2	2
179035	4	323	358	320	0	0	123	102	0	0	0	0	0	0	73	72	73	72	58	50	58	50	0	0	0	0	1732	68.2	217	195	3	2
179035	4	312	357	357	121	92	0	0	0	0	0	0	0	0	73	76	73	76	57	64	57	64	0	0	0	0	1778	70	202	204	4	2
179049	9	270	373	366	47	61	99	110	32	73	0	0	0	0	80	70	58	62	60	60	34	38	1	0	54	0	1948	76 7	175	183	1	9
179049	10	342	521	514	128	124	281	274	179	106	0	0	0	0	102	110	93	91	93	91	54	48	2	3	0	0	3156	124.3	642	620	2	9
179049	9	430	575	600	200	178	183	320	140	160	0	0	0	0	110	110	81	103	120	93	60	65	0	1	0	0	3529	138.9	856	876	3	9
179049	16	375	625	595	191	187	302	257	178	254	200	0	0	0	114	114	98	121	171	133	105	92	0	0	197	0	4310	170	899	846	4	9
179051	2	260	204	235	0	0	0	0	0	0	0	0	0	0	48	52	48	52	48	52	48	52	0	0	0	0	1099	43.3	62	71	1	2
179051	6	301	321	274	34	39	75	57	0	0	0	0	0	0	79	75	68	63	54	38	54	38	0	0	0	0	1570	61.8	182	148	2	2
179051	7	367	387	354	50	47	103	97	36	0	0	0	0	0	92	94	78	81	69	59	34	59	0	0	0	0	2007	79	295	287	3	2
179051	7	410	432	385	67	67	137	117	86	0	0	0	0	0	102	105	89	89	83	67	54	67	0	0	0	0	2354	93	417	389	4	2
179053	3	256	221	210	79	0	0	0	0	0	0	0	0	0	52	49	52	49	45	49	45	49	0	0	0	0	1156	45.5	75	59	1	3
179053	5	294	350	335	0	0	109	124	32	0	0	0	0	0	65	64	64	53	54	30	36	30	0	0	0	0	1640	64.6	170	163	2	3
179053	6	295	376	349	37	160	140	0	75	0	0	0	0	0	72	74	75	74	65	57	43	30	0	0	0	0	1922	75.7	235	207	3	3
179053	6	325	398	375	57	152	152	0	70	0	0	0	0	0	79	76	76	76	64	57	48	57	0	0	0	0	2063	81	248	219	4	3
179054	2	235	190	198	0	0	0	0	0	0	0	0	0	0	41	44	41	44	41	44	41	44	0	0	0	0	963	37.9	40	44	1	2
179054	4	366	325	340	0	0	69	80	0	0	0	0	0	0	57	62	57	62	38	46	38	46	0	0	0	0	1586	62.4	141	160	2	2
179054	7	448	420	419	47	48	179	160	0	58	0	0	0	0	92	93	86	75	61	68	61	38	0	0	0	0	2353	92.6	307	312	3	2
179054	8	462	425	470	51	48	203	175	0	76	0	0	0	0	95	102	86	83	60	73	60	48	0	0	102	0	2617	103	372	372	4	2
179055	2	231	245	230	0	0	0	0	0	0	0	0	0	0	44	45	44	45	44	45	44	45	0	0	0	0	1062	41.8	48	54	1	2
179055	5	396	369	372	0	43	147	101	0	0	0	0	0	0	63	97	63	63	52	43	52	43	0	0	0	0	1904	75	195	188	2	2
179055	6	385	479	429	42	55	212	124	0	0	0	0	0	0	98	106	84	71	60	50	60	50	0	0	0	0	2305	90.7	356	279	3	2
179055	7	424	420	490	57	73	229	178	95	0	0	0	0	0	102	108	86	83	70	64	57	64	0	0	0	0	2598	102	412	373	4	2
179064	4	235	236	255	0	0	32	36	0	0	0	0	0	0	44	44	44	44	27	33	27	33	0	0	0	0	1090	42.9	49	53	1	4
179064	8	335	387	372	31	39	127	134	120	92	0	0	0	0	71	70	66	64	63	60	46	36	0	0	0	0	2113	83.2	185	174	2	4
179064	8	341	415	422	87	62	141	147	166	137	0	0	0	0	77	74	80	72	75	69	52	50	0	0	0	0	2467	97.1	242	233	3	4
179064	8	360	460	455	89	38	175	156	140	137	0	0	0	0	76	73	76	76	73	70	48	48	0	0	0	0	2548	100	253	232	4	4
179068	2	214	177	172	0	0	0	0	0	0	0	0	0	0	38	39	38	39	38	39	38	39	0	0	0	0	871	34.3	29	29	1	2
179068	8	323	353	348	49	45	103	83	62	35	0	0	0	0	69	73	62	61	56	48	40	32	0	0	0	0	1842	72.5	177	162	2	2
179068	8	370	425	424	82	82	147	149	126	103	0	0	0	0	82	83	74	72	68	63	47	41	0	0	0	0	2438	96	305	288	3	2
179068	8	400	460	440	89	111	165	178	143	130	0	0	0	0	86	92	79	76	76	70	57	51	0	0	0	0	2703	106	359	332	4	2

PID	PTS	SPD	MBL	MBR	LG1	RG1	LG2	RG2	LG3	RG3	LG4	RG4	LG5	RG5	LH1	RH1	LH2	RH2	LH3	RH3	LH4	RH4	LAP	RAP	LAL	RAL	BCSM	BCSI	AWL	AWR	SET	YPT
179087	5	120	152	167	52	50	0	26	0	0	0	0	0	0	59	57	59	50	49	31	49	31	0	0	0	0	952	37.5	51	49	1	5
179087	6	283	264	327	101	0	112	131	0	51	0	0	0	0	73	78	69	68	62	67	51	45	0	0	0	0	1782	70.2	168	203	2	5
179087	8	302	374	397	115	129	175	178	141	72	0	0	0	0	90	89	80	80	79	69	54	48	0	0	0	0	2472	97.3	312	322	3	5
179087	8	350	411	400	140	143	171	175	111	64	0	0	0	0	92	95	79	83	79	76	57	54	0	0	0	0	2580	102	353	364	4	5
179093	5	187	211	216	27	28	43	0	0	0	0	0	0	0	68	56	50	56	33	45	33	45	0	0	0	0	1098	43.2	66	59	1	5
179093	8	333	360	336	44	57	168	181	101	71	0	0	0	0	79	83	74	74	63	60	44	34	0	0	0	0	2162	85.1	257	259	2	5
179093	8	400	443	424	76	81	200	218	176	144	0	0	0	0	99	99	94	95	89	80	66	56	0	0	0	0	2840	111.8	492	479	3	5
179093	9	445	503	475	102	98	210	235	213	191	67	0	0	0	105	105	98	102	95	95	83	70	0	0	0	0	3290	130	624	603	4	5
179102	2	76	58	55	0	0	0	0	0	0	0	0	0	0	32	33	32	33	32	33	32	33	0	0	0	0	449	17.7	7	8	1	2
179102	2	172	194	166	0	0	0	0	0	0	0	0	0	0	40	37	40	37	40	37	40	37	0	0	0	0	840	33.1	26	33	2	2
179102	4	250	316	326	0	0	70	89	0	0	0	0	0	0	58	55	58	55	40	38	40	38	0	0	0	0	1433	56.4	103	109	3	2
179102	4	280	401	409	130	162	0	0	0	0	0	0	0	0	67	67	67	67	54	57	54	57	0	0	0	0	1871	74	177	191	4	2
179105	2	63	13	4	0	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	0	0	0	0	80	3.1	.	.	1	2
179105	4	219	264	266	0	0	28	29	0	0	0	0	0	0	56	58	56	58	29	31	29	31	0	0	0	0	1154	45.4	77	84	2	2
179105	4	302	335	329	0	0	86	104	0	0	0	0	0	0	68	73	68	73	43	42	43	42	0	0	0	0	1608	63 3	140	142	3	2
179105	6	308	385	376	48	38	137	127	0	0	0	0	0	0	79	79	76	76	54	54	54	54	0	0	0	0	1945	77	208	206	4	2
179107	2	90	60	72	0	0	0	0	0	0	0	0	0	0	33	34	33	34	33	34	33	34	0	0	0	0	490	19.3	10	8	1	2
179107	6	238	351	321	0	0	185	159	91	67	0	0	0	0	63	61	60	54	56	32	47	32	0	0	0	0	1817	71.5	186	154	2	2
179107	8	340	457	416	56	39	196	210	95	113	0	0	0	0	77	75	68	66	66	64	59	54	0	0	0	0	2451	96.5	286	260	3	2
179107	9	400	500	442	79	70	229	203	165	146	44	0	0	0	86	89	79	79	79	79	73	64	0	0	0	0	2907	114	396	363	4	2
179110	3	227	276	265	0	0	78	0	0	0	0	0	0	0	70	55	55	55	36	55	36	55	0	0	0	0	1263	49.7	82	100	1	3
179110	6	414	484	465	58	74	205	213	0	0	0	0	0	0	94	100	84	85	71	77	50	77	0	0	0	0	2551	100 4	423	414	2	3
179110	5	357	354	312	39	0	62	0	0	0	0	0	0	0	107	95	78	95	55	95	55	95	0	2	0	0	1801	70.9	256	247	3	3
179110	10	375	465	453	67	191	83	89	0	105	0	0	0	0	114	95	92	95	64	57	64	57	0	0	197	0	2661	105	402	564	4	3
180007	2	61	45	64	0	0	0	0	0	0	0	0	0	0	25	28	25	28	25	28	25	28	0	0	0	0	382	15	6	4	1	2
180007	4	255	295	282	0	0	87	81	0	0	0	0	0	0	53	52	35	52	46	40	46	40	0	0	0	0	1364	53.7	98	95	2	2
180007	5	330	361	363	0	0	145	169	46	0	0	0	0	0	71	66	54	66	34	45	34	45	0	0	0	0	1829	72	178	189	3	2
180007	6	400	412	412	44	0	146	187	73	0	0	0	0	0	76	73	70	73	64	54	44	54	0	0	0	0	2183	86	245	237	4	2
180012	8	250	317	314	72	59	203	174	0	83	0	0	0	0	79	76	70	68	55	61	30	42	0	1	0	30	1984	78.1	206	214	1	8
180012	10	372	426	446	130	141	208	214	188	187	0	0	0	0	87	86	86	73	82	77	64	55	1	1	0	0	2924	115.1	454	455	2	8
180012	8	385	462	473	137	125	265	250	209	215	0	0	0	0	95	103	88	88	89	85	61	65	0	0	0	0	3195	125.8	577	541	3	8
180012	10	403	528	546	140	105	267	276	235	235	0	0	0	0	98	105	89	92	98	95	70	70	0	0	95	0	3547	140	621	619	4	8
180022	7	273	287	308	103	71	98	102	0	32	0	0	0	0	76	75	56	65	66	59	66	59	0	0	0	0	1796	70.7	181	206	1	7
180022	8	362	452	357	136	130	205	230	163	135	0	0	0	0	93	90	81	83	92	84	75	69	0	0	0	0	2837	111.7	506	451	2	7
180022	9	395	505	515	148	138	215	265	185	212	111	0	0	0	104	105	85	89	100	93	90	74	0	0	0	0	3429	135	643	639	3	7
180022	10	419	520	540	130	178	225	267	197	222	114	86	0	0	102	105	89	92	105	102	92	86	0	0	0	0	3670	144	650	744	4	7
180032	2	70	16	3	0	0	0	0	0	0	0	0	0	0	18	12	18	12	18	12	18	12	0	0	0	0	209	8.2	.	.	1	2
180032	2	237	217	219	0	0	0	0	0	0	0	0	0	0	48	48	48	48	48	48	48	48	0	0	0	0	1057	41 6	52	55	2	2
180032	.	.	295	319		.		.	.	.	.	.	.	.	.	.	.	.	.	.		.	.	.	0	.	.	.	106	114	3	2
180032	4	380	321	347	83	48	0	0	0	0	0	0	0	0	70	64	41	35	41	35	41	35	0	0	0	0	1540	61	146	141	4	2
181007	3	145	169	185	42	0	0	0	0	0	0	0	0	0	52	39	52	39	37	39	37	39	0	0	0	0	875	34.4	33	32	1	3

PID	PTS	SPD	MBL	MBR	LG1	RG1	LG2	RG2	LG3	RG3	LG4	RG4	LG5	RG5	LH1	RH1	LH2	RH2	LH3	RH3	LH4	RH4	LAP	RAP	LAL	RAL	BCSM	BCSI	AWL	AWR	SET	YPT
181007	8	267	333	295	37	39	157	150	81	38	0	0	0	0	69	68	58	57	53	49	40	21	0	0	0	0	1812	71.3	162	137	2	3
181007	8	310	429	391	62	71	204	214	126	145	0	0	0	0	83	80	72	71	64	68	50	50	0	0	0	0	2490	98 031	282	297	3	3
181007	10	306	466	453	76	98	219	244	191	152	51	38	0	0	92	92	76	79	76	73	64	60	0	0	0	0	2908	114	349	343	4	3
182047	5	201	255	251	26	0	53	93	0	0	0	0	0	0	68	56	51	56	40	38	40	38	0	0	0	0	1266	49.8	90	106	1	5
182047	8	316	407	442	114	25	175	174	103	150	0	0	0	0	80	87	71	70	62	69	45	51	0	0	0	0	2441	96.1	278	282	2	5
182047	8	365	433	461	140	124	192	200	134	155	0	0	0	0	94	96	80	82	77	81	59	66	0	0	0	0	2839	111 8	443	478	3	5
182047	12	360	408	435	178	124	194	194	130	54	0	146	0	0	98	105	89	95	89	102	70	108	0	0	95	0	3073	121	461	537	4	5
182058	4	230	275	256	28	0	90	0	0	0	0	0	0	0	72	52	56	52	40	52	40	52	0	0	0	0	1295	51	100	77	1	4
182058	8	335	372	358	69	49	199	196	117	101	0	0	0	0	83	81	71	74	65	66	42	40	0	0	0	0	2318	91 3	257	251	2	4
182058	9	394	421	425	86	84	246	241	126	155	0	24	0	0	98	100	85	86	82	78	51	64	0	0	0	0	2846	112	435	439	3	4
182058	9	410	481	451	102	95	279	279	171	140	35	0	0	0	114	105	98	95	89	83	73	57	0	0	0	0	3158	124	598	524	4	4
183023	6	208	249	277	79	71	66	59	0	0	0	0	0	0	71	74	54	55	45	45	45	45	0	0	0	0	1443	56.8	102	108	1	6
183023	8	278	386	393	115	108	123	110	39	74	0	0	0	0	83	84	65	73	65	87	36	46	0	0	0	0	2165	85.2	240	262	2	6
183023	8	358	449	480	140	141	199	169	173	129	0	0	0	0	103	102	85	84	116	84	75	55	0	0	0	0	2942	115.8	493	469	3	6
183023	9	335	468	469	152	140	165	191	156	146	0	0	0	0	102	108	86	86	130	92	67	54	0	0	44	0	2990	118	504	508	4	6
184002	7	227	280	280	56	47	145	125	37	0	0	0	0	0	78	78	70	70	64	53	35	53	0	0	0	0	1698	66.9	180	146	1	7
184002	7	277	379	389	43	60	209	198	0	49	0	0	0	0	101	87	84	81	64	68	64	38	0	0	0	0	2191	86.3	290	291	2	7
184002	9	357	442	448	95	93	264	232	114	156	0	0	0	0	107	102	92	88	79	80	49	56	1	0	0	0	2855	112 4	512	461	3	7
184002	9	375	451	479	89	86	270	229	76	175	0	0	0	0	108	105	98	95	76	89	51	67	0	0	117	0	3035	120	574	587	4	7
184003	9	332	234	289	26	55	153	146	77	32	0	0	0	0	83	80	68	65	60	55	40	44	1	0	43	0	1883	74 1	171	176	1	9
184003	8	404	394	388	96	78	198	216	165	171	0	0	0	0	104	98	79	86	72	79	48	51	0	0	0	0	2727	107 4	367	375	2	9
184003	8	397	408	429	85	88	206	221	181	186	0	0	0	0	103	102	85	85	78	79	52	57	0	0	0	0	2842	111.9	382	424	3	9
184003	10	427	426	406	95	95	254	235	194	200	0	0	0	0	102	111	89	92	79	83	57	57	0	0	83	0	3085	121	502	525	4	9
184014	9	320	294	330	62	51	103	109	107	35	0	0	0	0	82	93	70	70	92	59	40	34	1	0	120	0	2072	81.6	220	200	1	8
184014	8	348	440	449	100	116	169	176	92	115	0	0	0	0	98	99	85	84	76	72	46	52	0	0	0	0	2617	103	393	403	2	8
184014	8	401	461	464	130	130	173	166	128	153	0	0	0	0	103	110	81	81	77	83	52	57	0	0	0	0	2850	112.2	438	461	3	8
184014	10	355	399	476	86	165	257	175	114	108	0	0	0	0	137	111	108	86	89	76	64	64	0	0	241	0	3110	122	610	525	4	8
184024	5	236	285	281	26	0	0	89	0	0	0	0	0	0	79	59	79	48	48	37	48	37	2	0	250	0	1604	63.1	135	118	1	6
184024	9	384	500	504	40	182	241	232	153	157	0	0	0	0	87	106	78	81	81	69	52	47	0	2	0	0	2996	118	402	494	2	6
184024	8	382	558	562	130	132	280	254	209	154	0	0	0	0	101	96	86	81	88	83	68	55	0	0	0	0	3319	130.7	570	530	3	6
184024	8	450	600	564	130	156	311	314	229	191	0	0	0	0	95	95	89	89	92	86	73	67	0	0	0	0	3630	143	675	659	4	6
184029	6	323	325	332	65	62	114	120	0	0	0	0	0	0	85	90	69	69	54	60	54	60	0	0	0	0	1882	74.1	200	202	1	6
184029	8	401	413	440	90	97	161	152	64	60	0	0	0	0	98	99	84	87	76	80	52	45	0	0	0	0	2499	98.4	367	370	2	6
184029	8	404	456	439	87	92	188	193	122	81	0	0	0	0	96	102	83	82	82	76	57	55	0	0	0	0	2695	106.1	433	405	3	6
184029	9	425	437	413	111	111	184	165	83	95	25	0	0	0	102	114	95	102	130	102	73	64	0	0	0	0	2831	111	485	487	4	6
184040	7	275	348	335	85	101	205	160	135	0	0	0	0	0	86	81	72	69	98	49	48	49	0	0	0	0	2196	86.5	266	219	1	7
184040	8	341	489	489	106	128	228	240	233	227	0	0	0	0	98	104	82	83	82	81	63	62	0	0	0	0	3136	123.5	477	495	2	7
184040	10	350	505	491	152	132	236	268	290	260	135	0	0	0	105	110	91	90	95	85	82	70	1	0	0	0	3548	139 7	684	604	3	7
184040	10	397	527	508	162	152	213	260	222	197	121	0	0	0	111	124	95	98	95	89	83	79	0	0	60	0	3594	142	736	758	4	7
184057	6	197	226	209	0	60	115	59	31	0	0	0	0	0	69	65	59	57	47	45	30	45	0	0	0	0	1314	51.7	113	102	1	6
184057	8	303	356	371	196	106	172	180	122	84	0	0	0	0	98	85	72	74	70	69	49	49	0	0	0	0	2456	96.7	364	330	2	6

PID	PTS	SPD	MBL	MBR	LG1	RG1	LG2	RG2	LG3	RG3	LG4	RG4	LG5	RG5	LH1	RH1	LH2	RH2	LH3	RH3	LH4	RH4	LAP	RAP	LAL	RAL	BCSM	BCSI	AWL	AWR	SET	YPT
184057	10	365	441	415	210	166	205	225	177	147	0	0	0	0	110	108	86	89	80	81	64	60	1	1	0	0	3031	119 3	597	555	3	6
184057	9	420	466	468	254	248	248	222	156	146	0	0	0	0	111	108	92	92	86	95	54	54	0	0	67	0	3386	133	716	733	4	6
186005	7	342	373	357	87	88	101	53	80	0	0	0	0	0	77	75	61	55	53	42	40	42	0	0	0	0	1926	75 8	183	139	1	7
186005	9	469	460	461	95	119	127	170	187	179	0	70	0	0	91	93	78	80	90	85	64	69	0	0	0	0	2987	117.6	393	407	2	7
186005	9	532	545	525	149	134	215	231	219	154	80	0	0	0	106	102	89	81	87	80	79	58	0	0	0	0	3466	136.5	589	525	3	7
186005	10	539	601	566	146	130	159	213	203	191	127	25	0	0	108	108	89	89	98	92	86	76	0	0	0	0	3646	144	658	612	4	7
186007	8	257	322	334	38	26	135	150	81	109	0	0	0	0	73	72	59	60	49	54	37	37	0	0	0	0	1893	74.5	141	157	1	8
186007	9	358	487	481	52	55	168	222	194	151	0	0	0	0	78	79	76	78	71	69	60	54	0	1	0	0	2734	107.6	360	367	2	8
186007	9	458	573	580	77	85	242	248	261	243	0	0	0	0	98	105	89	90	86	85	65	60	1	0	0	0	3446	135.7	643	659	3	8
186007	12	501	566	535	86	98	248	279	213	229	0	0	0	0	117	111	102	102	102	98	79	79	0	0	194	0	3739	147		.	4	8
186026	8	240	236	252	51	48	110	135	45	27	0	0	0	0	73	72	54	57	53	51	30	35	0	0	0	0	1569	61.8	119	104	1	8
186026	8	308	354	343	67	87	210	189	139	116	0	0	0	0	91	84	77	74	89	76	49	50	0	0	0	0	2403	94 6	302	269	2	8
186026	9	348	371	377	82	89	229	210	145	150	0	0	0	0	99	98	84	84	86	100	50	55	1	0	0	0	2658	104.6	396	398	3	8
186026	9	381	418	441	98	105	264	248	229	175	32	0	0	0	102	102	89	89	171	108	67	64	0	0	0	0	3180	125	518	500	4	8
186036	8	256	358	339	46	45	94	100	87	84	0	0	0	0	72	73	60	61	57	55	40	40	0	0	0	0	1867	73.5	160	148	1	8
186036	8	333	445	442	50	45	130	153	131	97	0	0	0	0	78	76	72	70	67	62	53	43	0	0	0	0	2347	92 4	276	262	2	8
186036	8	410	472	491	101	60	129	180	159	175	0	0	0	0	91	90	77	81	75	78	57	66	0	0	0	0	2792	109 9	391	407	3	8
186036	10	485	548	538	127	102	213	194	146	213	143	111	0	0	95	95	92	89	89	86	95	76	0	0	0	0	3536	139	631	620	4	8
186119	5	229	276	299	0	0	101	94	0	38	0	0	0	0	53	53	53	54	50	36	50	36	0	0	0	0	1422	56	100	107	1	5
186119	8	374	427	420	62	54	195	216	98	99	0	0	0	0	77	77	71	70	67	67	40	43	0	0	0	0	2457	96 7	299	304	2	5
186119	8	405	485	472	90	47	239	279	135	115	0	0	0	0	102	101	85	85	81	76	49	40	0	0	0	0	2886	113.6	521	521	3	5
186119	8	407	478	548	92	92	289	289	140	137	0	0	0	0	102	102	92	92	86	89	57	54	0	0	0	0	3144	124	625	659	4	5
186121	8	285	290	300	64	42	127	97	43	26	0	0	0	0	66	69	59	59	55	54	35	35	0	0	0	0	1706	67.2	122	113	1	8
186121	9	374	416	413	65	68	194	184	160	146	0	49	0	0	80	83	71	70	69	76	58	64	0	0	0	0	2640	103.9	287	293	2	8
186121	9	362	449	461	76	89	235	226	203	92	66	0	0	0	100	103	89	87	85	81	70	68	0	0	0	0	2942	115 8	470	452	3	8
186121	10	440	506	518	102	111	283	298	194	200	48	102	0	0	121	111	102	102	95	95	86	89	0	0	0	0	3601	142	615	677	4	8
187003	6	200	227	278	0	57	59	142	0	0	0	0	0	0	58	67	50	60	32	45	32	45	2	0	181	0	1535	60.4	103	122	1	7
187003	6	327	331	350	92	66	184	196	0	0	0	0	0	0	69	78	69	68	57	53	40	53	0	0	0	0	2033	80	198	196	2	7
187003	7	465	444	402	106	84	236	155	170	0	0	0	0	0	98	87	78	69	71	50	52	50	0	0	0	0	2617	103	390	283	3	7
187003	8	405	455	453	114	83	232	244	181	181	0	0	0	0	98	95	86	86	76	79	54	54	0	0	0	0	2977	117	419	429	4	7
187037	2	87	14	18	0	0	0	0	0	0	0	0	0	0	26	25	26	25	26	25	26	25	0	0	0	0	323	12.7	1	1	1	2
187037	2	104	60	131	0	0	0	0	0	0	0	0	0	0	50	38	50	38	26	38	26	38	0	0	0	0	599	23 6	12	23	2	2
187037	.	.	214	235		.	.	.	.	.	.	.		.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	61	74	3	2
187037	6	250	295	307	44	25	64	64	0	0	0	0	0	0	73	76	64	67	44	48	44	48	0	0	0	0	1512	60	134	142	4	2
187038	2	95	100	74	0	0	0	0	0	0	0	0	0	0	34	29	34	29	34	29	34	29	0	0	0	0	521	20 5	8	13	1	2
187038	4	192	241	240	0	0	44	41	0	0	0	0	0	0	62	61	62	61	36	37	36	37	0	0	0	0	1150	45.3	73	77	2	2
187038	6	240	302	309	45	37	88	106	0	0	0	0	0	0	74	74	70	72	45	46	45	46	0	0	0	0	1599	63	143	152	3	2
187038	6	276	345	351	92	76	98	124	0	0	0	0	0	0	79	79	73	79	54	57	54	57	0	0	0	0	1896	75	194	216	4	2
187056	6	247	295	309	67	47	113	131	0	0	0	0	0	0	70	67	55	59	41	42	41	42	0	0	0	0	1626	64	115	133	1	6
187056	5	.	358	458	74	0	0	153	0	0	0	0	0	0	73	70	73	70	61	58	61	58	1	0	0	0	0	0	287	236	2	6
187056	8	450	531	530	159	129	228	221	211	173	0	0	0	0	99	96	87	91	85	89	70	66	0	0	0	0	3315	130.5	563	528	3	6

PID	PTS	SPD	MBL	MBR	LG1	RG1	LG2	RG2	LG3	RG3	LG4	RG4	LG5	RG5	LH1	RH1	LH2	RH2	LH3	RH3	LH4	RH4	LAP	RAP	LAL	RAL	BCSM	BCSI	AWL	AWR	SET	YPT
187056	9	462	562	565	159	175	251	254	257	229	0	0	0	0	111	114	95	95	98	98	76	70	0	0	0	0	3672	145	730	686	4	6
187057	8	266	377	333	68	55	134	155	89	85	0	0	0	0	76	69	68	64	60	56	39	35	0	0	0	0	2029	79.9	186	167	1	8
187057	8	358	428	443	106	114	205	190	186	186	0	0	0	0	90	89	78	77	77	77	57	50	0	0	0	0	2811	110.7	332	330	2	8
187057	8	439	520	486	109	111	251	232	210	236	0	0	0	0	102	98	89	85	88	85	56	60	0	0	0	0	3257	128.2	516	497	3	8
187057	8	494	565	555	143	156	314	289	222	251	0	0	0	0	111	108	98	95	95	92	60	60	0	0	0	0	3710	146	671	663	4	8
187069	8	313	320	302	62	54	123	119	97	88	0	0	0	0	71	74	63	65	60	60	47	44	0	0	0	0	1962	77.2	178	157	1	8
187069	8	377	434	415	76	82	210	127	167	167	0	0	0	0	90	85	79	80	75	75	62	59	0	0	0	0	2660	104.7	357	340	2	8
187069	11	485	493	506	131	132	243	201	252	240	126	180	0	30	110	108	94	97	99	100	85	91	0	0	0	0	3803	149.7	704	718	3	8
187069	10	495	500	512	156	146	273	225	229	219	111	210	0	0	105	105	105	95	102	146	86	98	0	0	0	0	3917	154	697	716	4	8
187082	5	155	249	206	94	0	81	0	0	0	0	0	0	0	70	74	59	74	42	47	42	47	0	1	0	138	1379	54.3	115	89	1	5
187082	8	326	415	412	125	140	132	124	45	64	0	0	0	0	85	92	72	69	61	65	46	48	0	0	0	0	2321	91.4	282	274	2	5
187082	9	433	504	515	177	203	176	188	118	134	0	0	0	0	102	108	88	85	88	84	63	61	0	1	0	0	3128	123.1	536	587	3	5
187082	11	440	557	576	165	225	203	206	130	114	0	0	0	0	124	121	95	92	92	86	64	64	0	0	143	0	3497	138	748	828	4	5
188006	8	332	335	338	77	55	141	123	41	59	0	0	0	0	78	79	68	70	57	61	31	35	0	0	0	0	1980	78	190	194	1	8
188006	8	442	453	466	99	103	204	183	93	49	0	0	0	0	91	92	80	81	77	72	47	37	0	0	0	0	2669	105.1	380	369	2	8
188006	8	497	542	559	167	142	266	253	143	93	0	0	0	0	115	110	98	94	84	86	55	47	0	0	0	0	3351	131.9	723	668	3	8
188006	11	473	586	577	184	171	270	244	102	162	0	0	0	0	114	114	98	102	86	95	51	67	0	0	203	0	3700	146	766	756	4	8
188018	2	186	228	213	0	0	0	0	0	0	0	0	0	0	44	43	44	43	44	43	44	43	0	0	0	0	975	38.4	53	48	1	2
188018	2	307	320	327	0	0	0	0	0	0	0	0	0	0	58	58	58	58	58	58	58	58	0	0	0	0	1418	55 8	106	107	2	2
188018	4	366	379	354	0	0	120	85	0	0	0	0	0	0	64	62	64	62	43	32	43	32	0	0	0	0	1706	67.2	202	177	3	2
188018	5	422	434	415	48	130	130	0	0	0	0	0	0	0	83	73	73	73	57	54	57	54	0	0	0	0	2103	83	276	246	4	2
188030	7	276	305	322	35	26	92	61	60	0	0	0	0	0	67	65	59	54	54	41	41	41	0	0	0	0	1599	63	112	99	1	7
188030	6	340	416	409	0	0	180	165	123	101	0	0	0	0	81	75	78	65	71	48	60	48	0	0	0	0	2260	89	280	246	2	7
188030	9	395	468	480	59	32	224	253	233	170	54	0	0	0	101	93	92	95	88	81	74	58	0	0	0	0	3050	120.1	498	446	3	7
188030	9	428	489	490	83	44	238	302	238	171	127	0	0	0	102	105	95	105	92	86	83	57	0	0	0	0	3334	131	598	552	4	7
188074	2	143	146	146	0	0	0	0	0	0	0	0	0	0	37	39	37	39	37	39	37	39	0	0	0	0	739	29.1	24	28	1	2
188074	5	294	284	284	26	0	88	88	0	0	0	0	0	0	66	62	62	62	45	41	45	41	0	0	0	0	1488	58.6	113	103	2	2
188074	6	318	350	325	58	42	153	160	0	0	0	0	0	0	80	76	73	72	51	51	51	51	0	0	0	0	1911	75.2	216	208	3	2
188074	6	351	378	375	64	25	159	181	0	0	0	0	0	0	86	86	79	79	64	60	64	60	0	0	0	0	2110	83	250	252	4	2
188080	6	245	340	347	0	87	137	103	0	0	0	0	0	0	67	71	63	58	46	44	46	44	1	0	48	0	1747	68.8	148	137	1	6
188080	7	356	472	477	120	121	235	186	0	122	0	0	0	0	79	79	73	72	65	67	65	48	0	0	0	0	2637	103.8	327	333	2	6
188080	9	427	603	622	190	184	281	261	0	188	0	0	0	0	94	94	90	89	78	80	78	57	1	2	0	0	3419	134.6	646	740	3	6
188080	15	427	568	588	213	203	311	292	187	206	0	0	0	0	102	105	95	95	89	89	57	73	0	0	445	0	4145	163	790	852	4	6
188085	4	241	302	324	0	0	138	109	0	0	0	0	0	0	64	67	64	62	45	53	45	53	0	0	0	0	1567	61.7	141	138	1	4
188085	8	399	483	471	60	55	194	196	158	130	0	0	0	0	88	86	78	76	75	73	68	67	0	0	0	0	2757	108.5	424	383	2	4
188085	7	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	3	4
188085	10	455	545	584	92	117	168	216	178	175	44	0	0	0	111	114	105	98	98	95	92	92	0	0	51	0	3432	135	834	846	4	4
189005	6	295	316	319	63	68	116	145	0	0	0	0	0	0	70	73	61	61	55	53	41	36	0	0	0	0	1772	69.8	150	169	1	6
189005	8	384	449	408	79	90	189	145	90	0	0	0	0	0	93	88	72	69	76	68	50	68	0	1	0	0	2419	95.2	326	315	2	6
189005	8	385	407	430	88	85	212	186	129	94	0	0	0	0	100	90	75	80	76	71	52	55	0	0	0	0	2615	103	352	358	3	6
189005	8	428	488	501	111	102	260	219	108	124	0	0	0	0	102	102	89	89	79	83	54	44	0	0	0	0	2982	117	462	482	4	6

PID	PTS	SPD	MBL	MBR	LG1	RG1	LG2	RG2	LG3	RG3	LG4	RG4	LG5	RG5	LH1	RH1	LH2	RH2	LH3	RH3	LH4	RH4	LAP	RAP	LAL	RAL	BCSM	BCSI	AWL	AWR	SET	YPT
189006	4	258	340	351	0	0	130	157	0	0	0	0	0	0	57	55	57	55	45	40	45	40	0	0	0	0	1630	64.2	120	115	1	4
189006	8	435	474	446	50	40	212	220	140	154	0	0	0	0	92	90	72	73	65	66	45	47	0	0	0	0	2721	107.1	287	281	2	4
189006	8	437	501	495	60	62	271	255	143	176	0	0	0	0	95	102	82	85	69	75	42	52	0	0	0	0	3002	118.2	388	388	3	4
189006	8	445	508	507	76	89	289	286	162	108	0	0	0	0	105	105	89	86	83	76	57	48	0	0	0	0	3117	123	454	472	4	4
189010	6	272	325	341	26	38	171	129	0	0	0	0	0	0	73	75	69	70	61	66	61	49	0	0	0	0	1826	71 9	199	204	1	6
189010	10	464	454	480	95	98	175	164	158	84	0	106	0	0	103	106	87	86	80	95	61	78	1	0	0	0	2975	117.1	453	481	2	6
189010	11	475	505	530	122	125	256	231	170	192	0	32	0	0	119	117	98	100	86	99	74	88	4	2	0	0	3425	134 8	762	732	3	6
189010	15	372	558	562	133	171	175	171	235	200	171	73	0	0	127	124	105	102	105	127	121	92	0	0	327	0	4051	159	906	870	4	6
189013	3	214	194	210	0	0	28	0	0	0	0	0	0	0	49	48	49	48	25	48	25	48	0	0	0	0	986	38.8	63	63	1	3
189013	7	375	326	380	79	71	124	135	0	57	0	0	0	0	87	90	71	74	58	65	58	42	0	0	0	0	2092	82.4	217	242	2	3
189013	8	407	397	406	155	100	160	170	31	110	0	0	0	0	110	105	80	86	70	76	37	60	0	0	0	0	2560	100.8	386	418	3	3
189013	8	440	419	409	171	133	171	162	117	171	0	0	0	0	117	111	95	98	83	95	64	79	0	0	0	0	2938	116	518	538	4	3
189017	8	310	374	328	66	72	143	134	81	56	0	0	0	0	78	80	66	65	60	59	41	39	0	0	0	0	2052	80.8	225	197	1	8
189017	9	417	499	466	116	116	229	224	223	173	56	0	0	0	101	99	90	87	85	78	73	55	0	0	0	0	3187	125.5	562	488	2	8
189017	8	405	502	486	160	118	251	218	212	189	0	0	0	0	113	105	95	91	85	88	63	67	0	0	0	0	3248	127.9	634	570	3	8
189017	8	415	432	433	124	124	206	200	124	121	0	0	0	0	98	102	92	89	86	83	57	60	0	0	0	0	2845	112	458	436	4	8
189021	7	.	135	330	95	60	26	120	0	58	0	0	0	0	71	76	53	64	33	58	33	40	0	0	0	0	0	0	76	186	1	7
189021	10	489	466	451	88	89	225	210	168	90	0	0	0	0	98	92	90	89	93	90	56	54	1	1	0	0	2940	115.7	494	449	2	7
189021	10	513	511	525	101	90	252	211	216	230	0	0	0	0	112	109	100	95	106	108	73	75	1	1	0	0	3429	135	769	728	3	7
189021	9	560	572	560	133	111	260	251	200	241	0	0	0	0	117	111	111	105	114	114	73	76	0	0	38	0	3749	148	796	788	4	7
189029	7	295	344	338	74	60	166	167	37	0	0	0	0	0	71	75	65	65	55	53	35	53	0	0	0	0	1953	76.9	206	200	1	7
189029	8	443	470	466	119	91	165	203	128	113	0	0	0	0	79	80	65	68	61	63	48	50	0	0	0	0	2712	106 8	298	306	2	7
189029	8	475	490	498	104	95	252	260	170	169	0	0	0	0	92	91	79	81	75	75	57	51	0	0	0	0	3114	122.6	482	496	3	7
189029	9	611	537	528	146	159	279	241	191	194	0	0	0	0	105	105	92	89	86	83	64	70	0	0	114	0	3692	145	688	698	4	7
189044	6	193	267	251	38	52	136	143	0	0	0	0	0	0	70	70	58	60	45	45	45	45	0	0	0	0	1518	59.8	120	121	1	6
189044	6	414	407	441	95	84	213	247	0	0	0	0	0	0	103	101	77	78	60	65	60	65	0	0	0	0	2510	98.8	324	366	2	6
189044	8	433	465	459	80	66	260	265	122	131	0	0	0	0	102	101	85	84	71	73	47	44	0	0	0	0	2888	113 7	488	450	3	6
189044	7	422	494	434	83	0	305	267	143	117	0	0	0	0	102	92	89	92	76	86	51	51	0	0	0	0	2903	114	554	464	4	6
189050	9	300	279	305	57	46	124	92	80	65	0	30	0	0	68	70	65	61	63	90	42	68	0	0	0	0	1905	75	166	170	1	9
189050	8	429	447	474	90	83	249	237	161	135	0	0	0	0	90	91	90	87	90	82	51	57	0	0	0	0	2943	115.9	473	500	2	9
189050	9	420	478	461	110	121	268	260	131	155	0	0	0	0	95	96	94	106	91	101	70	75	1	0	0	0	3133	123.3	636	642	3	9
189050	12	478	537	508	124	152	292	286	200	213	32	25	0	0	111	111	111	114	108	152	86	86	0	0	127	0	3853	152	918	944	4	9
189072	4	238	245	262	0	0	45	60	0	0	0	0	0	0	65	56	53	56	39	42	39	42	0	0	0	0	1242	48.9	83	91	1	4
189072	7	364	412	420	54	41	157	196	0	56	0	0	0	0	95	86	73	80	61	68	61	46	0	0	0	0	2270	89.4	270	301	2	4
189072	8	450	485	492	92	55	207	222	65	117	0	0	0	0	110	96	82	90	69	80	49	57	0	0	0	0	2818	110.9	444	468	3	4
189072	9	430	495	496	86	76	210	187	149	130	0	0	0	0	108	105	92	89	89	86	60	70	0	0	35	0	2993	118	580	536	4	4
189077	6	241	278	289	78	67	81	84	0	0	0	0	0	0	68	68	58	56	42	40	42	40	0	0	0	0	1532	60.3	129	125	1	6
189077	8	365	415	415	118	93	190	182	134	96	0	0	0	0	88	91	76	75	119	69	56	44	0	0	0	0	2626	103.4	325	297	2	6
189077	8	405	451	447	163	109	213	194	66	92	0	0	0	0	100	95	82	85	74	76	39	49	0	0	0	0	2740	107.9	440	402	3	6
189077	9	417	459	470	165	124	219	191	76	89	0	0	0	0	98	98	89	86	79	79	51	54	0	0	51	0	2895	114	492	464	4	6
189080	3	198	280	277	0	0	43	0	0	0	0	0	0	0	57	64	57	64	35	64	35	64	0	0	0	0	1238	48.7	89	98	1	3

PID	PTS	SPD	MBL	MBR	LG1	RG1	LG2	RG2	LG3	RG3	LG4	RG4	LG5	RG5	LH1	RH1	LH2	RH2	LH3	RH3	LH4	RH4	LAP	RAP	LAL	RAL	BCSM	BCSI	AWL	AWR	SET	YPT
189080	6	316	384	390	77	102	191	167	0	0	0	0	0	0	87	83	74	73	52	49	52	49	0	0	0	0	2146	84 5	264	249	2	3
189080	8	377	407	455	138	137	269	244	80	0	0	0	0	0	99	100	86	85	72	69	38	69	0	1	0	0	2726	107.3	440	416	3	3
189080	8	423	470	461	171	181	257	232	0	0	0	0	0	0	98	98	86	89	67	70	67	70	0	0	67	0	2907	114	480	486	4	3
189090	4	218	261	255	0	0	90	88	0	0	0	0	0	0	57	58	57	58	43	43	43	43	0	0	0	0	1314	51.7	95	91	1	4
189090	7	319	291	352	0	42	189	178	70	79	0	0	0	0	79	75	70	68	60	59	54	31	0	0	0	0	2016	79.4	201	202	2	4
189090	8	432	510	461	91	89	259	266	192	154	0	0	0	0	107	100	85	81	76	74	58	52	0	0	0	0	3087	121.5	524	470	3	4
189090	8	416	448	424	83	76	213	213	102	102	0	0	0	0	102	98	79	76	70	70	51	48	0	0	0	0	2669	105	338	318	4	4
189091	4	180	210	188	0	0	38	40	0	0	0	0	0	0	62	58	62	58	40	39	40	39	0	0	0	0	1054	41.5	60	74	1	4
189091	8	437	380	400	70	75	175	176	40	84	0	0	0	0	97	90	78	81	70	74	56	61	0	0	0	0	2444	96.2	270	308	2	4
189091	8	473	415	472	87	91	208	225	83	134	0	0	0	0	96	103	80	85	75	82	60	71	0	0	0	0	2840	111.8	390	468	3	4
189091	9	492	485	502	105	95	235	251	156	178	0	0	0	0	108	105	92	95	89	89	73	76	0	0	41	0	3267	129	544	598	4	4
189102	5	224	227	232	0	61	37	62	0	0	0	0	0	0	60	67	49	53	35	40	35	40	0	0	0	0	1222	48.1	74	88	1	5
189102	6	376	388	368	129	66	149	145	0	0	0	0	0	0	80	77	69	73	54	58	54	58	0	0	0	0	2144	84 4	241	231	2	5
189102	8	426	409	452	190	128	168	167	36	71	0	0	0	0	95	91	77	81	66	76	46	51	0	0	0	0	2630	103.5	376	400	3	5
189102	8	500	458	477	203	171	184	191	0	73	0	0	0	0	95	95	83	86	67	76	48	57	0	0	0	0	2864	113	426	464	4	5
189103	7	240	272	218	51	58	75	125	0	37	0	0	0	0	65	72	55	60	46	49	46	35	0	0	0	0	1504	59.2	109	103	1	7
189103	8	395	429	433	135	127	250	229	178	166	0	0	0	0	95	93	78	79	75	76	48	46	0	0	0	0	2932	115.4	377	361	2	7
189103	9	470	516	524	149	155	265	240	210	218	0	30	0	0	94	92	90	89	91	65	60	42	0	0	0	0	3400	133 9	528	528	3	7
189103	11	552	439	538	181	178	270	264	200	206	206	54	0	0	114	108	89	92	133	92	102	76	0	0	38	0	3932	155	674	640	4	7
189106	6	270	294	293	47	55	117	107	0	0	0	0	0	0	65	70	55	51	41	44	41	44	0	0	0	0	1594	62 8	123	118	1	6
189106	8	437	414	413	81	80	219	204	133	140	0	0	0	0	85	87	73	75	65	70	44	50	0	0	0	0	2670	105.1	319	329	2	6
189106	8	482	497	518	106	89	256	228	229	276	0	0	0	0	101	100	90	90	83	88	68	69	0	0	0	0	3370	132.7	570	612	3	6
189106	9	592	536	547	102	98	191	222	248	203	67	0	0	0	108	108	95	95	89	92	79	70	0	0	0	0	3542	139	710	692	4	6
189108	8	147	248	235	59	42	79	88	33	55	0	0	0	0	64	61	54	57	50	60	24	34	0	0	0	0	1390	54.7	103	108	1	8
189108	11	333	459	471	124	97	190	228	191	195	112	0	0	0	95	103	85	88	112	91	82	64	1	2	0	0	3123	123	508	504	2	8
189108	11	405	500	535	132	38	286	160	230	203	54	0	0	0	110	109	96	95	100	112	80	81	1	3	0	0	3330	131.1	780	694	3	8
189108	13	432	582	548	171	175	270	276	251	241	0	156	0	0	121	121	111	108	117	130	89	108	0	0	194	0	4200	165	1010	1058	4	8
189117	8	301	325	339	98	78	123	165	80	96	0	0	0	0	75	77	64	68	53	62	40	43	0	0	0	0	2087	82.2	203	213	1	8
189117	10	454	489	510	98	97	217	250	230	211	83	0	0	0	93	90	87	83	83	80	71	57	1	0	0	0	3284	129.3	554	508	2	8
189117	11	463	556	569	121	125	225	212	270	282	162	160	0	0	102	102	94	98	92	94	83	80	2	0	0	0	3892	153.2	810	849	3	8
189117	11	500	540	544	130	114	235	238	225	251	143	121	0	0	108	114	102	105	102	102	98	89	0	0	73	0	3934	155	902	954	4	8
190030	6	299	286	281	60	55	114	59	0	0	0	0	0	0	69	57	49	47	33	32	33	32	0	0	0	0	1506	59.3	103	91	1	6
190030	6	444	442	446	71	83	240	187	0	0	0	0	0	0	85	83	72	73	52	50	52	50	0	0	0	0	2430	95.7	298	282	2	6
190030	7	557	571	575	120	120	291	288	0	118	0	0	0	0	101	101	85	85	66	74	66	49	0	0	0	0	3267	128.6	558	586	3	6
190030	6	530	570	589	130	124	289	267	0	0	0	0	0	0	111	111	92	92	70	67	70	67	0	0	0	0	3178	125	650	652	4	6
190035	6	138	237	221	66	71	80	72	0	0	0	0	0	0	58	55	55	52	39	38	39	38	0	0	0	0	1259	49.6	81	91	1	6
190035	6	213	304	292	68	77	120	125	0	0	0	0	0	0	66	69	60	61	56	54	56	54	0	0	0	0	1675	65.9	148	150	2	6
190035	8	270	375	360	122	121	164	169	106	80	0	0	0	0	84	81	79	78	85	80	46	40	0	0	0	0	2340	92.1	310	296	3	6
190035	8	280	422	415	165	127	210	181	127	102	0	0	0	0	89	83	86	86	92	89	57	57	0	0	0	0	2666	105	402	372	4	6
190039	8	323	362	362	65	52	135	143	32	38	0	0	0	0	80	77	66	71	59	58	47	44	0	0	0	0	2014	79 3	197	197	1	8
190039	8	382	443	455	146	123	184	165	92	104	0	0	0	0	93	94	78	88	73	79	53	56	0	0	0	0	2708	106 6	388	394	2	8

PID	PTS	SPD	MBL	MBR	LG1	RG1	LG2	RG2	LG3	RG3	LG4	RG4	LG5	RG5	LH1	RH1	LH2	RH2	LH3	RH3	LH4	RH4	LAP	RAP	LAL	RAL	BCSM	BCSI	AWL	AWR	SET	YPT
190039	8	439	516	530	160	134	227	210	98	135	0	0	0	0	105	105	92	85	84	86	57	60	0	0	0	0	3123	123	566	584	3	8
190039	9	472	562	571	159	159	254	232	133	124	0	0	0	0	117	111	92	92	89	92	60	64	0	0	48	0	3431	135	668	690	4	8
190040	7	285	364	335	182	91	151	222	0	146	0	0	0	0	85	85	74	71	67	64	49	44	0	0	0	0	2315	91 1	278	273	1	7
190040	9	400	491	483	189	164	260	239	151	169	52	0	0	0	101	97	85	82	84	78	69	57	0	0	0	0	3251	128	534	490	2	7
190040	11	438	512	499	192	189	268	299	208	231	77	73	0	0	114	124	96	98	94	97	81	79	1	0	0	0	3770	148 4	722	722	3	7
190040	9	482	533	530	159	248	283	292	197	197	0	0	0	0	117	117	102	98	98	102	67	83	0	0	32	0	3736	147	796	832	4	7
190041	6	320	346	361	57	50	111	111	0	0	0	0	0	0	72	69	60	60	54	52	54	52	0	0	0	0	1829	72	180	186	1	6
190041	8	485	490	501	118	127	190	223	99	47	0	0	0	0	89	103	81	82	86	86	52	39	0	0	0	0	2898	114 1	476	452	2	6
190041	9	501	590	562	161	163	315	295	162	174	0	0	0	0	112	122	106	102	114	100	64	66	0	1	0	0	3710	146 1	908	870	3	6
190041	15	435	630	515	143	102	305	171	83	276	0	0	0	0	117	127	121	111	111	111	76	127	0	0	489	0	4050	159	1040	938	4	6
190043	9	280	364	357	91	79	186	171	50	76	75	0	0	0	79	78	72	72	90	72	65	43	0	0	0	0	2300	90 6	238	232	1	9
190043	8	363	437	430	125	115	185	168	191	140	0	0	0	0	95	90	87	85	205	113	68	60	0	0	0	0	2957	116.4	428	400	2	9
190043	8	407	423	409	155	147	155	197	0	36	0	0	0	0	110	106	101	100	78	100	78	77	1	0	0	0	2680	105 5	608	564	3	9
190043	12	406	405	465	213	187	171	200	0	0	0	0	0	0	175	108	98	105	102	83	102	83	0	0	610	0	3511	138	.	.	4	9
190055	2	210	217	201	0	0	0	0	0	0	0	0	0	0	52	43	52	43	52	43	52	43	0	0	0	0	1008	39 7	65	58	1	2
190055	4	331	356	354	0	0	113	101	0	0	0	0	0	0	76	75	70	71	50	48	50	48	0	0	0	0	1743	68 6	178	172	2	2
190055	6	396	428	407	0	0	160	155	92	27	0	0	0	0	88	86	82	65	69	38	47	38	0	0	0	0	2178	85 7	334	284	3	2
190055	8	417	455	457	51	51	181	175	140	76	0	0	0	0	92	92	89	86	79	73	54	51	0	0	0	0	2618	103	416	374	4	2
190068	7	241	344	332	91	79	101	124	0	42	0	0	0	0	83	79	70	66	41	54	41	38	0	0	0	0	1826	71.9	176	183	1	7
190068	8	399	448	436	137	120	219	147	52	37	0	0	0	0	92	101	78	76	64	78	40	43	0	0	0	0	2567	101.1	356	338	2	7
190068	8	423	476	441	137	130	238	249	58	154	0	0	0	0	100	108	86	89	69	79	40	51	0	0	0	0	2928	115.3	436	490	3	7
190068	7	379	497	483	102	140	267	279	0	143	0	0	0	0	114	121	92	95	67	83	67	51	0	0	0	0	2978	117	480	584	4	7
190072	2	155	182	165	0	0	0	0	0	0	0	0	0	0	47	41	47	41	47	41	47	41	0	0	0	0	854	33 6	44	34	1	2
190072	6	323	311	318	0	36	161	143	90	0	0	0	0	0	75	77	68	67	58	49	34	49	0	0	0	0	1859	73.2	185	160	2	2
190072	6	372	341	362	45	58	153	146	0	0	0	0	0	0	83	82	73	73	59	50	59	50	0	0	0	0	2006	79	218	226	3	2
190072	8	397	406	405	60	73	222	168	60	38	0	0	0	0	92	89	83	79	67	64	38	35	0	0	0	0	2376	94	324	310	4	2
190073	2	198	257	230	0	0	0	0	0	0	0	0	0	0	41	43	41	43	41	43	41	43	0	0	0	0	1021	40.2	70	58	1	2
190073	6	368	348	369	27	43	118	115	0	0	0	0	0	0	76	74	62	66	41	44	41	44	0	0	0	0	1836	72.3	160	170	2	2
190073	6	393	409	406	64	32	156	159	0	0	0	0	0	0	77	84	68	72	50	55	50	28	0	0	0	0	2103	82 8	224	228	3	2
190073	8	428	444	433	86	70	152	178	64	89	0	0	0	0	86	86	76	76	64	67	41	44	0	0	0	0	2483	98	302	316	4	2
190074	2	172	208	195	0	0	0	0	0	0	0	0	0	0	44	45	44	45	44	45	44	45	0	0	0	0	931	36.7	43	47	1	2
190074	4	229	260	274	0	0	95	118	0	0	0	0	0	0	55	59	55	59	33	40	33	40	0	0	0	0	1350	53.1	94	110	2	2
190074	4	305	285	308	0	0	0	147	0	0	0	0	0	0	54	78	54	69	54	40	54	40	1	0	0	0	1489	58 6	102	172	3	2
190074	8	381	384	332	54	0	181	0	0	0	0	0	0	0	108	76	83	76	51	76	51	76	0	0	232	0	2161	85	274	222	4	2
190078	8	218	305	307	60	65	129	105	0	41	0	0	0	0	75	73	62	63	50	54	50	40	1	0	33	0	1731	68.1	167	155	1	8
190078	8	350	392	363	70	78	86	44	110	0	0	0	0	0	85	82	76	66	67	45	45	45	1	0	0	0	2005	78.9	270	188	2	8
190078	10	360	462	430	99	104	241	221	188	160	0	0	0	0	103	103	98	94	88	88	61	63	1	1	0	0	2965	116.7	552	496	3	8
190078	10	367	503	442	140	108	260	257	219	203	0	0	0	0	114	114	102	105	92	95	70	73	0	0	187	0	3452	136	680	656	4	8
190083	5	213	266	258	0	0	78	107	45	0	0	0	0	0	59	64	51	58	34	41	34	41	0	0	0	0	1349	53.1	100	92	1	5
190083	7	306	420	406	0	32	75	158	100	93	0	0	0	0	76	74	72	76	63	66	43	47	0	0	0	0	2107	83	240	232	2	5
190083	8	351	465	470	66	71	232	185	163	181	0	0	0	0	87	85	80	80	70	77	52	54	0	0	0	0	2769	109	392	390	3	5

PID	PTS	SPD	MBL	MBR	LG1	RG1	LG2	RG2	LG3	RG3	LG4	RG4	LG5	RG5	LH1	RH1	LH2	RH2	LH3	RH3	LH4	RH4	LAP	RAP	LAL	RAL	BCSM	BCSI	AWL	AWR	SET	YPT
190083	8	380	496	455	38	92	216	168	168	178	0	0	0	0	95	92	89	86	83	79	64	67	0	0	0	0	2845	112	476	454	4	5
190087	6	250	286	286	26	0	82	98	45	0	0	0	0	0	58	60	56	58	55	48	38	48	0	0	0	0	1494	58.8	106	101	1	6
190087	8	394	401	398	76	91	151	129	96	90	0	0	0	0	75	75	71	68	67	65	47	51	0	0	0	0	2345	92.3	238	220	2	6
190087	8	440	451	460	108	106	220	215	119	136	0	0	0	0	88	89	81	81	77	78	51	55	0	0	0	0	2855	112.4	374	388	3	6
190087	9	490	491	494	127	121	219	140	184	222	0	108	0	0	95	95	86	89	89	95	70	86	0	0	0	0	3301	130	510	516	4	6
190091	3	165	225	221	0	0	0	26	0	0	0	0	0	0	47	50	47	50	47	30	47	30	0	0	0	0	985	38.8	54	59	1	3
190091	5	313	300	305	48	0	11	114	0	0	0	0	0	0	71	62	69	62	44	45	44	45	0	0	0	0	1533	60.4	130	132	2	3
190091	7	342	374	377	59	76	222	203	125	0	0	0	0	0	90	91	78	75	69	58	39	58	0	0	0	0	2336	92	290	272	3	3
190091	8	330	372	366	73	95	244	216	130	111	0	0	0	0	89	92	83	79	73	73	41	41	0	0	0	0	2509	99	318	312	4	3
190098	6	190	323	314	42	32	97	109	0	0	0	0	0	0	72	71	63	64	48	45	48	45	0	0	0	0	1563	61.5	135	136	1	6
190098	6	344	455	453	112	114	128	178	0	0	0	0	0	0	83	84	72	72	55	52	55	52	0	0	0	0	2309	90.9	274	276	2	6
190098	8	347	515	525	116	124	252	265	145	172	0	0	0	0	92	98	86	88	69	76	49	52	0	0	0	0	3071	120.9	448	512	3	6
190098	11	356	568	584	149	152	292	292	197	216	0	0	0	0	114	111	98	98	86	89	60	60	0	0	124	0	3648	144	684	748	4	6

APPENDIX D.

Fluctuating Asymmetry Measures

Appendix D - Fluctuating asymmetry measures for main beam length (MBA), total normal tine length (TGA), total tine length (TTA), total main beam circumference (THA), gross Boone and Crockett scores (GBCA), antler weight (AWA), and abnormal tine length (APA) for 144 male white-tailed deer from the Kerr Wildlife Management Area. Deer identification number (PID), deer age (AGE), number of yearling points (YPT), and yearling antler type (YRT) are shown.

PID	AGE	YPT	YRT	MBA	TGA	TTA	THA	GBCA	AWA	APA
100016	1	8	F	-0.045	-0.179	-0.179	-0.039	-0.077	-0.034	0.00
100016	2	8	F	-0.008	0.064	0.064	-0.041	0.005	0.004	0.00
100016	3	8	F	-0.023	-0.065	-0.065	-0.055	-0.048	0.027	0.00
100016	4	8	F	-0.019	-0.198	-0.198	-0.053	-0.096	-0.058	0.00
100017	1	2	S	.	.	.	.	.		.
100017	2	2	S	0.194	0.000	0.000	-0.039	0.083	0.146	0.00
100017	3	2	S	-0.005	0.095	0.095	-0.105	0.000	-0.170	0.00
100017	4	2	S	0.041	0.171	0.171	-0.074	0.043	-0.177	0.00
100040	1	2	S	-0.548	.		0.066	-0.197	-0.207	0.00
100040	2	2	S	-0.214	0.468	0.468	0.073	0.009	0.018	0.00
100040	3	2	S	0.021	0.200	0.200	-0.033	0.046	0.075	0.00
100040	4	2	S	-0.037	-0.096	-0.096	-0.022	-0.049	0.058	0.00
107007	1	6	F	-0.026	-0.320	-0.320	-0.058	-0.090	0.349	0.00
107007	2	6	F	0.148	0.070	0.070	-0.084	0.056	0.190	0.00
107007	3	6	F	-0.135	-0.739	-0.739	-0.004	-0.277	-0.164	0.00
107007	4	6	F	0.131	0.697	0.697	0.023	0.278	0.021	0.00
173004	1	4	F	0.039	-0.507	-0.507	-0.222	-0.111	0.038	0.00
173004	2	4	F	0.010	-0.636	-0.636	-0.063	-0.190	-0.037	0.00
173004	3	4	F	-0.024	-0.021	-0.021	-0.027	-0.024	-0.020	0.00
173004	4	4	F	0.027	0.075	-0.014	0.032	0.012	0.104	-2.00
173005	1	3	F	.	.	.	.	.	.	.
173005	2	3	F	-0.022	-0.429	-0.429	0.055	-0.135	0.139	0.00
173005	3	3	F	-0.063	.	.	.	.	-0.069	.
173005	4	3	F	0.016	0.040	-0.001	-0.017	0.001	-0.019	-2.00
173007	1	4	F	0.124	0.351	0.351	0.072	0.134	0.160	0.00
173007	2	4	F	-0.071	-0.075	-0.075	0.028	-0.043	.	0.00
173007	3	4	F	.	.	.				.
173007	4	4	F	0.031	2.000	0.718	0.149	0.245		-2.00
173009	1	2	S	0.098	.		0.105	0.103	-0.267	0.00
173009	2	2	S	0.069	-0.052	-0.052	0.050	0.033	-0.011	0.00
173009	3	2	S	-0.095	0.430	0.430	-0.069	0.039	0.044	0.00
173009	4	2	S	0.067	0.169	0.169	-0.016	0.079	0.027	0.00
173023	1	2	S	-0.089	.		-0.056	-0.069	-0.207	0.00
173023	2	2	S	-0.015	-0.392	-0.392	-0.026	-0.143	-0.094	0.00
173023	3	2	S	-0.026	-0.020	-0.020	-0.073	-0.037	-0.019	0.00
173023	4	2	S	0.037	0.002	0.002	0.012	0.017	0.015	0.00
173034	1	4	F	0.362	.	.	.		0.121	.
173034	2	4	F	0.021	.	.	.		-0.011	.
173034	3	4	F	0.011	-0.321	-0.321	-0.072	-0.112	-0.028	0.00
173034	4	4	F	0.044	-0.060	-0.060	0.026	0.005	0.020	0.00
173041	1	2	S	-0.035	.	.	0.085	0.033	0.216	0.00
173041	2	2	S	0.008	-0.127	-0.127	-0.010	-0.011	0.017	0.00
173041	3	2	S	0.015	0.137	0.137	-0.010	0.021	-0.036	0.00

PID	AGE	YPT	YRT	MBA	TGA	TTA	THA	GBCA	AWA	APA
173041	4	2	S	0.030	-2.000	-2.000	0.127	-0.084	-0.075	0.00
173046	1	2	S	0.988	.	.	0.857	0.906	1.429	0.00
173046	2	2	S	0.028	-0.106	-0.106	0.137	0.034	0.019	0.00
173046	3	2	S	-0.013	0.062	0.062	0.023	0.023	0.015	0.00
173046	4	2	S	0.009	0.007	-0.097	0.042	-0.021	0.029	-2.00
173068	1	2	S	0.745	.	.	0.141	0.405	-1.097	0.00
173068	2	2	S	0.024	0.237	0.237	-0.032	0.031	0.045	0.00
173068	3	2	S	0.035	0.076	0.076	0.084	0.062	0.060	0.00
173068	4	2	S	0.033	-0.069	-0.069	0.038	0.001	-0.003	0.00
173069	1	2	S	-0.072	.	.	-0.353	-0.272	0.222	0.00
173069	2	2	S	-0.019	-0.158	-0.158	-0.059	-0.059	-0.027	0.00
173069	3	2	S	0.042	.	.	.	.	-0.005	
173069	4	2	S	0.045	0.084	0.084	-0.097	0.017	0.008	0.00
173091	1	2	S	.	.	.	.	.	.	.
173091	2	2	S	.	.	.		.		
173091	3	2	S	.	.	.	.	.	.	.
173091	4	2	S	0.029	-0.049	-0.049	-0.027	-0.011	.	0.00
174038	1	6	F	-0.362	-2.000	-2.000	-0.066	-0.345	-0.345	0.00
174038	2	6	F	0.013	.	.	.	.	-0.011	.
174038	3	6	F	-0.017	0.111	0.111	0.052	0.041	-0.013	0.00
174038	4	6	F	-0.006	-0.739	-0.739	0.015	-0.125	0.027	0.00
174051	1	2	S	0.111	.	.	-0.020	0.048	0.154	0.00
174051	2	2	S	0.071	0.061	0.061	0.036	0.058	-0.031	0.00
174051	3	2	S	-0.011	0.260	0.260	0.162	0.121	-0.007	0.00
174051	4	2	S	0.020	-0.124	-0.536	0.091	-0.161	0.166	-2.00
174053	1	4	F	0.140	2.000	0.000	0.059	0.088	-0.557	-2.00
174053	2	4	F	0.014	0.580	0.580	0.045	0.158	0.139	0.00
174053	3	4	F	0.090	0.216	0.216	0.118	0.132	0.132	0.00
174053	4	4	F	0.062	0.190	0.080	-0.003	0.046	0.070	-2.00
174061	1	5	F	0.224	-0.171	-0.171	0.252	0.169	0.234	0.00
174061	2	5	F	0.199	.	.	.	.	0.098	.
174061	3	5	F	0.179	0.242	0.242	-0.003	0.136	0.053	0.00
174061	4	5	F	0.019	0.276	0.276	0.042	0.083	0.043	0.00
174093	1	4	F	-0.060	-0.245	-0.245	0.240	0.020	0.055	0.00
174093	2	4	F	0.039	0.062	0.062	-0.014	0.031	0.056	0.00
174093	3	4	F	-0.060	-0.193	-0.193	-0.087	-0.115	-0.068	0.00
174093	4	4	F	0.006	0.059	0.059	0.126	0.060	0.025	0.00
174094	1	6	F	-0.059	0.660	0.660	0.111	0.121	0.076	0.00
174094	2	6	F	-0.032	.	.	.	.	0.110	.
174094	3	6	F	0.010	0.083	0.083	0.017	0.036	0.050	0.00
174094	4	6	F	-0.027	-0.221	-0.221	0.000	-0.078	-0.053	0.00
174192	1	5	F	0.029	-0.145	-0.145	-0.010	-0.026	0.027	0.00
174192	2	5	F	-0.078	-0.502	-0.502	0.051	-0.161	-0.070	0.00
174192	3	5	F	0.002	0.244	0.244	0.027	0.114	-0.162	0.00
174192	4	5	F	0.123	0.034	0.034	0.061	0.072	0.170	0.00
175064	1	2	S	-0.224	.	.	0.000	-0.115	-0.261	0.00
175064	2	2	S	-0.059	-0.046	-0.046	-0.066	-0.059	0.324	0.00
175064	3	2	S	0.000	.	.	.	.	-0.060	
175064	4	2	S	-0.062	-0.246	-0.246	-0.028	-0.094	-0.175	0.00
176046	1	2	S	0.092	.	.	0.080	0.086	0.128	0.00
176046	2	2	S	0.103	0.368	0.368	0.073	0.167	0.222	0.00
176046	3	2	S	-0.013	0.290	0.290	-0.051	0.081	0.135	0.00
176046	4	2	S	-0.030	0.105	0.105	-0.032	0.024	0.025	0.00

PID	AGE	YPT	YRT	MBA	TGA	TTA	THA	GBCA	AWA	APA
177005	1	5	F	0.051	-0.574	-0.574	0.023	-0.080	-0.082	0.00
177005	2	5	F	0.004	0 505	0.505	0.115	0.188	-0 133	0.00
177005	3	5	F	0.041	-0.161	-0.161	0.019	-0.035	-0.013	0.00
177005	4	5	F	0.053	-0.185	-0.185	0.029	-0.036	-0.041	0 00
177009	1	6	F	0.011	-0.652	-0.652	0.051	-0.084	-0.020	0.00
177009	2	6	F	0.012	-0.012	-0.012	0.051	0.014	-0.054	0.00
177009	3	6	F	0.055	-0.157	-0.157	-0.061	-0.054	-0.027	0.00
177009	4	6	F	-0.042	-0.035	-0.035	-0.054	-0.042	-0 088	0.00
177014	1	7	F	-0.059	-0.296	-0.296	-0.035	-0.112	-0.102	0 00
177014	2	7	F	0.079	0.042	0.042	0.062	0.061	0.037	0 00
177014	3	7	F	0.058	0.055	0.055	0.028	0.049	-0 041	0.00
177014	4	7	F	0 062	0.132	0.085	-0.024	0.049	0.022	-2.00
177021	1	5	F	-0 059	0.931	0.931	0.275	0.195	0.040	0.00
177021	2	5	F	-0 045	-0.219	-0.219	-0.136	-0.124	-0.006	0.00
177021	3	5	F	0.049	-0.033	-0.033	0.026	0.012	0.116	0 00
177021	4	5	F	-0.078	0.046	0.046	-0 019	-0.011	-0 016	0.00
177023	1	4	F	-0.044	0.123	0.123	-0.037	-0.007	-0.010	0.00
177023	2	4	F	-0 022	0.209	0.209	0.086	0.091	0.122	0.00
177023	3	4	F	0.046	0.039	0.039	0.035	0 040	0.081	0.00
177023	4	4	F	-0 084	-0.147	-0.183	0.057	-0 093	-0.012	-2.00
177025	1	2	S	-0.420	.	.	0 029	-0.134	0.435	0 00
177025	2	2	S	-0.016	.	.	0.020	0.003	0.120	0.00
177025	3	2	S	0.041	.		-0.054	-0.007	0 047	0 00
177025	4	2	S	0 073	.	.	0.116	0.094	0.135	0.00
177033	1	4	F	0.005	-2.000	-2.000	0.165	-0.061	-0.036	0.00
177033	2	4	F	0.026	0.145	0.145	0.045	0 070	0.138	0.00
177033	3	4	F	0 002	0 068	0.068	0.042	0.036	0.045	0.00
177033	4	4	F	-0 037	-0.024	-0.024	0.047	-0.011	-0.037	0.00
177034	1	4	F	0.061	-0.362	-0.362	-0.101	-0.062	0.093	0.00
177034	2	4	F	-0.117	0 765	0.765	0.059	0.075	-0.014	0.00
177034	3	4	F	-0 028	-0 051	-0.051	0.030	-0.019	-0.060	0.00
177034	4	4	F	-0.059	-0.204	-0.204	-0.086	-0.123	-0.144	0.00
177037	1	2	S	0.108	.	.	.	.	.	.
177037	2	2	S	0 108	.	.	-0.345	-0.210	0.095	0.00
177037	3	2	S	0.344	0.905	0.905	0 036	0.269	0 513	0 00
177037	4	2	S	0.252	-0.027	-0 027	0.127	0.161	0.385	0 00
177043	1	2	S	-0.293	.		-0 182	-0 210	-0 286	0.00
177043	2	2	S	0.109	-2.000	-2.000	0 218	0.091	0 139	0.00
177043	3	2	S	-0 056	-0.014	-0.014	-0.147	-0.089	-0 023	0 00
177043	4	2	S	0 074	0.099	0.099	0.022	0 057	0.065	0.00
177046	1	5	F	-0 018	0.222	0 222	0.074	0.056	-0 032	0 00
177046	2	5	F	0 006	0.220	0.220	0.046	0.084	-0 016	0.00
177046	3	5	F	-0 005	0.086	0 086	0.003	0.027	0 062	0.00
177046	4	5	F	-0 009	0.017	0.017	0.000	0 003	0 038	0 00
177047	1	4	F	-0.009	.	.	.	.	0 051	.
177047	2	4	F	-0 024	.	.	.	.	0 005	
177047	3	4	F	-0 069	0.059	0.059	-0 023	-0.011	0.000	0 00
177047	4	4	F	-0.051	0.067	0 067	0.020	0.008	-0.005	0 00
178001	1	7	F	-0 046	-0 184	-0.184	0 077	-0.041	0.088	0.00
178001	2	7	F	0.160	0.415	0.415	-0 054	0.184	0.208	0 00
178001	3	7	F	0 124	0.197	0.197	0 036	0.123	-0 196	0.00
178001	4	7	F	0 013	-0.055	-0 362	-0.008	-0.153	-0 001	-2.00
178019	1	2	S	-0 150	.	.	-0.054	-0.100	0 242	0.00

PID	AGE	YPT	YRT	MBA	TGA	TTA	THA	GBCA	AWA	APA
178019	2	2	S	-0.007	-0.174	-0.174	0.004	-0.037	-0.072	0.00
178019	3	2	S	-0.033	-0.573	-0.573	0.118	-0.113	-0.148	0.00
178019	4	2	S	0.031	-0.142	-0.245	0.006	-0.052	-0.090	-2.00
178020	1	6	F	-0.093		.	.	.	0.055	.
178020	2	6	F	-0.013	.	.	.	.	-0.107	.
178020	3	6	F	0.020	.	.	.	.	-0.142	.
178020	4	6	F	0.000	-0.154	-0.490	-0.010	-0.245	-0.181	-2.00
178022	1	4	F	0.020	0.115	0.115	-0.021	0.014	0.099	0.00
178022	2	4	F	0.034	0.003	0.003	0.023	0.021	0 009	0.00
178022	3	4	F	0.030	-0.009	-0.009	0.037	0.017	0.061	0.00
178022	4	4	F	0.069	-0.163	-0.209	-0.080	-0.078	0.038	-2.00
178023	1	2	S	0.045	.	.	-0.105	-0.028	-0.018	0.00
178023	2	2	S	-0.037	0.116	0.116	0.031	0.008	-0.073	0.00
178023	3	2	S	-0.025	-0.009	-0.009	-0.030	-0.024	-0.106	0.00
178023	4	2	S	-0.032	0.230	0.230	-0.049	0.006	-0.035	0.00
178032	1	6	F	0.059	-0.322	-0.322	0.047	-0.034	-0 069	0.00
178032	2	6	F	-0.093	-0.071	-0.071	0.004	-0.061	-0.035	0.00
178032	3	6	F	-0.059	-0.111	-0.111	-0.022	-0.073	-0.080	0.00
178032	4	6	F	.	0.190	-0.095	0.039	.	0.149	-2.00
178034	1	6	F	0.055	0.007	0.007	0.021	0.033	0.012	0.00
178034	2	6	F	0.012	0.000	0.000	-0.021	-0.001	0.015	0.00
178034	3	6	F	0.002	-0.130	-0.130	-0.023	-0.052	-0.048	0.00
178034	4	6	F	0.016	0.007	0.007	-0.019	0.004	0.015	0.00
178035	1	8	F	-0.028	0.060	0.060	0.030	0.017	0.060	0.00
178035	2	8	F	0.037	-0.058	-0.058	0.007	-0.007	0.052	0.00
178035	3	8	F	0.060	-0.010	-0.010	0.067	0.036	0.027	0.00
178035	4	8	F	0.000	0.099	-0.092	0.219	0.023	-0.035	-2.00
178038	1	4	F	0.274	2.000	2.000	-0.097	0.231	-0.280	0.00
178038	2	4	F	-0.011	-0.229	-0 229	0.005	-0.061	0.000	0.00
178038	3	4	F	0.011	-0.140	-0.140	-0.043	-0.058	-0.054	0.00
178038	4	4	F	0.047	0.050	0.050	0.031	0.044	0.072	0.00
178039	1	2	S	-0.024	.	.	-0.091	-0.059	-0 027	0.00
178039	2	2	S	0.011	-0.404	-0.404	-0.115	-0.143	0.127	0.00
178039	3	2	S	-0.055	-0.119	-0.119	-0.038	-0.071	-0.045	0.00
178039	4	2	S	0.010	-0.026	-0.026	0.000	-0.006	-0.056	0.00
178041	1	8	F	-0.058	0.170	0.170	0.025	0.038	0.047	0.00
178041	2	8	F	-0.063	-0.011	-0.011	-0.018	-0.033	0.009	0.00
178041	3	8	F	-0.014	-0.175	-0.175	-0 058	-0.090	-0.036	0.00
178041	4	8	F	-0.013	-0.061	-0 061	-0.043	-0.040	-0.014	0.00
178045	1	2	S	-0.075	.		-0.026	-0.050	0.725	0.00
178045	2	2	S	-0.035	-0.074	-0.074	-0.031	-0.044	-0.066	0.00
178045	3	2	S	0 062	-0.123	-0.123	-0.026	-0.024	-0.050	0.00
178045	4	2	S	-0.024	0.094	0.094	0.027	0.031	-0.016	0.00
178049	1	2	S	0.204	.	.	0.076	0.140	-0.385	0.00
178049	2	2	S	0 019	0.055	0.055	0.036	0.032	0.055	0.00
178049	3	2	S	0.042	0.015	0.015	0.034	0.031	0.052	0.00
178049	4	2	S	0.071	0.033	0 033	0.028	0.046	0.093	0.00
178052	1	6	F	-0.060	-1.413	-1.413	0.054	-0.340	-0.490	0.00
178052	2	6	F	0.140	0 742	0.742	0.045	0.315	0 335	0.00
178052	3	6	F	0.026	0.038	0.038	0 078	0.043	0.061	0.00
178052	4	6	F	-0.021	0.039	0.002	-0.023	-0.011	0.023	-2.00
178053	1	6	F	-0.126	-0.431	-0.431	-0.113	-0.191	-0.131	0.00
178053	2	6	F	-0.021	0.078	0.078	-0.030	0 013	-0.050	0.00

PID	AGE	YPT	YRT	MBA	TGA	TTA	THA	GBCA	AWA	APA
178053	3	6	F	0.020	-0.185	-0.185	0.010	-0.059	0.081	0.00
178053	4	6	F	-0.003	0.087	0.087	-0.065	0.020	0.059	0.00
178063	1	2	S	-0.137	.	.	-0.027	-0.061	0.316	0.00
178063	2	2	S	-0.076	-0.595	-0.595	-0.109	-0.152	-0.131	0.00
178063	3	2	S	0.063	-0.364	-0.364	0.103	0.004	0.112	0.00
178063	4	2	S	-0.024	0.310	0.310	0.074	0.087	0.007	0.00
178067	1	2	S	-0.226		.	-0.026	-0.112	-0.333	0.00
178067	2	2	S	0.052	-0.121	-0.121	-0.030	-0.025	-0.025	0.00
178067	3	2	S	-0.008	-0.015	-0.015	0.010	-0.007	-0.021	0.00
178067	4	2	S	-0.184	-0.145	-0.145	0.044	-0.114	-0.169	0.00
178071	1	6	F	-0.059	0.063	0.063	-0.037	-0.028	-0.114	0.00
178071	2	6	F	0.033	0.323	0.323	-0.038	0.095	0.113	0.00
178071	3	6	F	-0.011	0.009	0.009	-0.106	-0.028	-0.012	0.00
178071	4	6	F	0.017	-0.131	-0.131	-0.035	-0.054	0.006	0.00
178079	1	2	S	-0.016	.	.	0.054	0.033	0.000	0.00
178079	2	2	S	-0.056	2.000	2.000	-0.203	0.018	-0.118	0.00
178079	3	2	S	-0.007	-0.075	-0.075	-0.045	-0.036	-0.062	0.00
178079	4	2	S	0.002	-0.159	-0.159	0.011	-0.040	-0.065	0.00
179006	1	4	F	0.060	-2.000	-2.000	0.103	-0.105	-0.107	0.00
179006	2	4	F	0.022	-0.248	-0.248	-0.036	-0.084	-0.006	0.00
179006	3	4	F	-0.034	0.072	0.072	0.022	0.017	-0.064	0.00
179006	4	4	F	0.007	-0.034	-0.034	0.000	-0.009	-0.009	0.00
179018	1	2	S	0.013	.	.	0.025	0.019	-1.135	0.00
179018	2	2	S	-0.003	-0.047	-0.047	-0.008	-0.014	-0.025	0.00
179018	3	2	S	0.039	-0.095	-0.095	-0.034	-0.024	-0.050	0.00
179018	4	2	S	-0.004	-0.221	-0.221	-0.030	-0.082	-0.075	0.00
179021	1	2	S	0.772	.	.	0.133	0.354	0.933	0.00
179021	2	2	S	0.056	0.255	0.255	0.005	0.065	0.065	0.00
179021	3	2	S	0.067	-0.252	-0.252	0.064	-0.004	-0.048	0.00
179021	4	2	S	0.003	-0.182	-0.182	-0.038	-0.068	-0.134	0.00
179027	1	2	S	-0.048	.	.	0.053	-0.008	0.000	0.00
179027	2	2	S	0.031	-0.211	-0.211	-0.047	-0.061	-0.070	0.00
179027	3	2	S	-0.036	0.157	0.157	0.007	0.037	0.003	0.00
179027	4	2	S	0.050	-0.033	-0.033	-0.010	0.006	0.015	0.00
179028	1	3	F	0.559	-2.000	-2.000	-0.151	0.027	-0.526	0.00
179028	2	3	F	-0.052	1.071	1.071	-0.162	0.069	0.199	0.00
179028	3	3	F	-0.026	2.000	2.000	-0.035	0.371	0.298	0.00
179028	4	3	F	0.099	0.634	0.223	0.097	0.142	0.261	-2.00
179032	1	3	F	-0.056	-2.000	-2.000	0.057	-0.087	.	0.00
179032	2	3	F	.	.	.	.	.	.	.
179032	3	3	F	0.000		.	.	.	-0.145	.
179032	4	3	F	0.006	-0.024	-0.682	-0.067	-0.361	-0.159	-2.00
179035	1	2	S	0.005		.	0.020	0.012	0.048	0.00
179035	2	2	S	-0.020	-0.029	-0.029	0.000	-0.014	0.007	0.00
179035	3	2	S	-0.112	-0.187	-0.187	-0.071	-0.109	-0.107	0.00
179035	4	2	S	0.000	-0.272	-0.272	0.074	-0.012	0.010	0.00
179049	1	9	F	-0.019	0.313	0.050	-0.009	0.004	0.045	-2.00
179049	2	9	F	-0.014	-0.154	-0.154	-0.006	-0.066	-0.035	0.00
179049	3	9	F	0.043	0.229	0.229	0.000	0.103	0.023	0.00
179049	4	9	F	-0.049	-0.221	-0.419	-0.059	-0.218	-0.061	-2.00
179051	1	2	S	0.141	.	.	0.080	0.112	0.135	0.00
179051	2	2	S	-0.158	-0.127	-0.127	-0.175	-0.159	-0.206	0.00
179051	3	2	S	-0.089	-0.270	-0.270	0.071	-0.071	-0.027	0.00

PID	AGE	YPT	YRT	MBA	TGA	TTA	THA	GBCA	AWA	APA
179051	4	2	S	-0 115	-0.447	-0.447	0.000	-0.157	-0.069	0.00
179053	1	3	F	-0.051	-2.000	-2.000	0.010	-0.196	-0.239	0.00
179053	2	3	F	-0.044	-0.128	-0.128	-0.212	-0.110	-0.042	0.00
179053	3	3	F	-0 074	-0.447	-0.447	-0.082	-0.171	-0.127	0.00
179053	4	3	F	-0.060	-0.589	-0.589	-0.004	-0.174	-0.124	0.00
179054	1	2	S	0.041		.	0.071	0.055	0.095	0.00
179054	2	2	S	0.045	0 148	0.148	0.128	0.085	0.126	0.00
179054	3	2	S	-0.002	0.163	0 163	-0.091	0.014	0 016	0.00
179054	4	2	S	0.101	0 163	-0.174	0.016	-0.006	0.000	-2.00
179055	1	2	S	-0.063		.	0.022	-0.026	0.118	0.00
179055	2	2	S	0.008	-0.021	-0.021	0.067	0.021	-0 037	0.00
179055	3	2	S	-0.110	-0.346	-0.346	-0.086	-0.156	-0.243	0.00
179055	4	2	S	0.154	-0.411	-0.411	0.013	-0.051	-0.099	0.00
179064	1	4	F	0.077	0.118	0.118	0.081	0.082	0 078	0 00
179064	2	4	F	-0 040	-0.048	-0.048	-0.067	-0 049	-0.061	0.00
179064	3	4	F	0.017	-0.130	-0.130	-0 069	-0.056	-0.038	0.00
179064	4	4	F	-0.011	-0 199	-0.199	-0.022	-0.077	-0.087	0.00
179068	1	2	S	-0 029	.		0.026	-0.003	0.000	0.00
179068	2	2	S	-0.014	-0.271	-0.271	-0.059	-0.091	-0.088	0.00
179068	3	2	S	-0 002	-0.061	-0.061	-0.045	-0.033	-0 057	0.00
179068	4	2	S	-0.044	0.054	0.054	-0.031	-0.006	-0.078	0 00
179087	1	5	F	0 094	0.375	0.375	-0.244	-0.019	-0.040	0.00
179087	2	5	F	0.213	-0 157	-0.157	0.012	0.047	0 189	0.00
179087	3	5	F	0.060	-0.128	-0.128	-0.058	-0.042	0.032	0.00
179087	4	5	F	-0.027	-0.100	-0.100	0.003	-0.045	0.031	0.00
179093	1	5	F	0.023	-0.857	-0 857	0.093	-0.042	-0 112	0.00
179093	2	5	F	-0 069	-0 013	-0 013	-0.035	-0.040	0.008	0.00
179093	3	5	F	-0.044	-0 020	-0.020	-0.053	-0.038	-0.027	0.00
179093	4	5	F	-0.057	-0.122	-0 122	-0.024	-0.074	-0.034	0.00
179102	1	2	S	-0.053		.	0.031	0.005	0.133	0.00
179102	2	2	S	-0.156	.	.	-0.078	-0.120	0.237	0.00
179102	3	2	S	0 031	0.239	0.239	-0.052	0.032	0.057	0.00
179102	4	2	S	0.020	0.219	0.219	0.024	0.058	0.076	0.00
179105	1	2	S	-1.059	.	.	.	.	.	0.00
179105	2	2	S	0.008	0.035	0.035	0.046	0.024	0.087	0.00
179105	3	2	S	-0.018	0.189	0.189	0.035	0.031	0 014	0.00
179105	4	2	S	-0 024	-0.114	-0.114	0 000	-0.035	-0.010	0.00
179107	1	2	S	0.182	.	.	0.030	0.080	-0.222	0.00
179107	2	2	S	-0.089	-0.199	-0.199	-0.232	-0.161	-0.188	0.00
179107	3	2	S	-0.094	0.042	0.042	-0.042	-0.035	-0.095	0.00
179107	4	2	S	-0 123	-0.209	-0.209	-0.019	-0.129	-0.087	0.00
179110	1	3	F	-0.041	-2 000	-2.000	0.110	-0.127	0.198	0 00
179110	2	3	F	-0 040	0 087	0 087	0.125	0.042	-0 022	0.00
179110	3	3	F	-0 126	-2.000	-2.000	0.252	-0.080	-0.036	0.00
179110	4	3	F	-0.026	0.879	0.104	-0.094	-0.003	0.335	-2.00
180007	1	2	S	0.349	.	.	0.113	0.193	-0 400	0.00
180007	2	2	S	-0.045	-0 071	-0.071	0 022	-0.027	-0.031	0.00
180007	3	2	S	0.006	-0.122	-0.122	0.140	0.012	0.060	0.00
180007	4	2	S	0.000	-0.338	-0.338	0.000	-0.085	-0.033	0.00
180012	1	8	F	-0 010	0.139	0 229	0.054	0.093	0.038	2.00
180012	2	8	F	0.046	0.030	0.030	-0.092	0.006	0 002	0.00
180012	3	8	F	0.024	-0.035	-0 035	0 024	-0.001	-0.064	0.00
180012	4	8	F	0 034	-0 041	-0.179	0.020	-0 061	-0.003	-2.00

PID	AGE	YPT	YRT	MBA	TGA	TTA	THA	GBCA	AWA	APA
180022	1	7	F	0.071	0.020	0.020	-0.023	0.025	0.129	0.00
180022	2	7	F	-0.235	-0.018	-0.018	-0.045	-0.096	-0.115	0.00
180022	3	7	F	0.020	-0.069	-0.069	-0.049	-0.034	-0.006	0.00
180022	4	7	F	0.038	0.123	0.123	-0.008	0.064	0.135	0.00
180032	1	2	S	-1.368	.	.	-0.400	-0.532	.	0.00
180032	2	2	S	0.009	.	.	0.000	0.005	0.056	0.00
180032	3	2	S	0.077	.	.	.	.	0.073	
180032	4	2	S	0.078	-0.534	-0.534	-0.133	-0.057	-0.035	0.00
181007	1	3	F	0.090	-2.000	-2.000	-0.132	-0.132	-0.031	0.00
181007	2	3	F	-0.121	-0.191	-0.191	-0.120	-0.144	-0.167	0.00
181007	3	3	F	-0.093	0.092	0.092	0.000	0.000	0.052	0.00
181007	4	3	F	-0.028	-0.009	-0.009	-0.013	-0.017	-0.017	0.00
182047	1	5	F	-0.016	0.163	0.163	-0.057	-0.002	0.163	0.00
182047	2	5	F	0.082	-0.116	-0.116	0.071	0.010	0.014	0.00
182047	3	5	F	0.063	0.028	0.028	0.047	0.045	0.076	0.00
182047	4	5	F	0.064	0.031	-0.142	0.169	0.009	0.152	-2.00
182058	1	4	F	-0.072	-2.000	-2.000	0.000	-0.257	-0.260	0.00
182058	2	4	F	-0.038	-0.107	-0.107	0.000	-0.053	-0.024	0.00
182058	3	4	F	0.009	0.096	0.096	0.037	0.051	0.009	0.00
182058	4	4	F	-0.064	-0.133	-0.133	-0.095	-0.100	-0.132	0.00
183023	1	6	F	0.106	-0.109	-0.109	0.018	0.028	0.057	0.00
183023	2	6	F	0.018	0.053	0.053	0.152	0.067	0.088	0.00
183023	3	6	F	0.067	-0.154	-0.154	-0.153	-0.074	-0.050	0.00
183023	4	6	F	0.002	0.008	-0.080	-0.124	-0.063	0.008	-2.00
184002	1	7	F	0.000	-0.322	-0.322	0.028	-0.080	-0.209	0.00
184002	2	7	F	0.026	0.197	0.197	-0.133	0.027	0.003	0.00
184002	3	7	F	0.013	0.017	0.017	-0.003	0.010	-0.105	0.00
184002	4	7	F	0.060	0.119	-0.119	0.067	-0.008	0.022	-2.00
184003	1	9	F	0.210	-0.094	-0.248	-0.028	-0.023	0.029	-2.00
184003	2	9	F	-0.015	0.013	0.013	0.036	0.009	0.022	0.00
184003	3	9	F	0.050	0.048	0.048	0.016	0.040	0.104	0.00
184003	4	9	F	-0.048	-0.024	-0.166	0.048	-0.075	0.045	-2.00
184014	1	8	F	0.115	-0.330	-0.671	-0.104	-0.216	-0.095	-2.00
184014	2	8	F	0.020	0.120	0.120	0.007	0.050	0.025	0.00
184014	3	8	F	0.006	0.041	0.041	0.056	0.032	0.051	0.00
184014	4	8	F	0.176	-0.020	-0.436	-0.166	-0.170	-0.150	-2.00
184024	1	6	F	-0.014	1.096	-1.025	-0.336	-0.387	-0.134	-2.00
184024	2	6	F	0.008	0.273	0.273	0.017	0.112	0.205	0.00
184024	3	6	F	0.007	-0.136	-0.136	-0.085	-0.070	-0.073	0.00
184024	4	6	F	-0.062	-0.014	-0.014	-0.035	-0.036	-0.024	0.00
184029	1	6	F	0.021	0.017	0.017	0.063	0.035	0.010	0.00
184029	2	6	F	0.063	-0.019	-0.019	0.003	0.021	0.008	0.00
184029	3	6	F	-0.038	-0.081	-0.081	-0.009	-0.045	-0.067	0.00
184029	4	6	F	-0.056	-0.083	-0.083	-0.046	-0.062	0.004	0.00
184040	1	7	F	-0.038	-0.478	-0.478	-0.203	-0.243	-0.194	0.00
184040	2	7	F	0.000	0.048	0.048	0.015	0.024	0.037	0.00
184040	3	7	F	-0.028	-0.208	-0.208	-0.049	-0.116	-0.124	0.00
184040	4	7	F	-0.037	-0.164	-0.244	0.016	-0.114	0.029	-2.00
184057	1	6	F	-0.078	-0.204	-0.204	0.034	-0.066	-0.102	0.00
184057	2	6	F	0.041	-0.279	-0.279	-0.042	-0.109	-0.098	0.00
184057	3	6	F	-0.061	-0.096	-0.096	-0.006	-0.062	-0.073	0.00
184057	4	6	F	0.004	-0.066	-0.163	0.017	-0.068	0.023	-2.00
186005	1	7	F	-0.044	-0.621	-0.621	-0.076	-0.202	-0.273	0.00

PID	AGE	YPT	YRT	MBA	TGA	TTA	THA	GBCA	AWA	APA
186005	2	7	F	0.002	0.272	0.272	0.012	0.106	0.035	0.00
186005	3	7	F	-0.037	-0.244	-0.244	-0.117	-0.139	-0.115	0.00
186005	4	7	F	-0.060	-0.127	-0.127	-0.043	-0.082	-0.072	0.00
186007	1	8	F	0.037	0.115	0.115	0.023	0.059	0.107	0.00
186007	2	8	F	-0.012	0.033	0.033	-0.018	0.003	0.019	0.00
186007	3	8	F	0.012	-0.007	-0.007	0.006	0.003	0.025	0.00
186007	4	8	F	-0.056	0.102	-0.200	-0.025	-0.109	.	-2.00
186026	1	8	F	0.066	0.019	0.019	0.024	0.038	-0.135	0.00
186026	2	8	F	-0.032	-0.059	-0.059	-0.075	-0.054	-0.116	0.00
186026	3	8	F	0.016	-0.015	-0.015	0.055	0.015	0.005	0.00
186026	4	8	F	0.054	-0.165	-0.165	-0.167	-0.099	-0.035	0.00
186036	1	8	F	-0.055	0.009	0.009	0.000	-0.021	-0.078	0.00
186036	2	8	F	-0.007	-0.053	-0.053	-0.073	-0.038	-0.052	0.00
186036	3	8	F	0.039	0.065	0.065	0.049	0.050	0.040	0.00
186036	4	8	F	-0.018	-0.014	-0.014	-0.070	-0.029	-0.018	0.00
186119	1	5	F	0.080	0.266	0.266	-0.140	0.045	0.068	0.00
186119	2	5	F	-0.017	0.039	0.039	0.008	0.009	0.017	0.00
186119	3	5	F	-0.027	-0.051	-0.051	-0.048	-0.041	0.000	0.00
186119	4	5	F	0.136	-0.006	-0.006	0.000	0.049	0.053	0.00
186121	1	8	F	0.034	-0.346	-0.346	0.009	-0.080	-0.077	0.00
186121	2	8	F	-0.007	0.065	0.065	0.053	0.035	0.021	0.00
186121	3	8	F	0.026	-0.351	-0.351	-0.015	-0.129	-0.039	0.00
186121	4	8	F	0.023	0.126	0.126	-0.017	0.056	0.096	0.00
187003	1	7	F	0.202	1.085	-0.187	0.231	0.083	0.169	-2.00
187003	2	7	F	0.056	-0.052	-0.052	0.070	0.026	-0.010	0.00
187003	3	7	F	-0.099	-0.727	-0.727	-0.155	-0.333	-0.318	0.00
187003	4	7	F	-0.004	-0.037	-0.037	0.000	-0.016	0.024	0.00
187037	1	2	S	0.250	.	.	-0.039	0.000	0.000	0.00
187037	2	2	S	0.743	.	.	0.000	0.287	0.629	0.00
187037	3	2	S	0.093	.	.	.	.	0.193	.
187037	4	2	S	0.040	-0.193	-0.193	0.060	0.011	0.058	0.00
187038	1	2	S	-0.299	.	.	-0.159	-0.216	0.476	0.00
187038	2	2	S	-0.004	-0.071	-0.071	0.000	-0.008	0.053	0.00
187038	3	2	S	0.023	0.072	0.072	0.017	0.031	0.061	0.00
187038	4	2	S	0.017	0.051	0.051	0.045	0.035	0.107	0.00
187056	1	6	F	0.046	-0.011	-0.011	0.014	0.022	0.145	0.00
187056	2	6	F	0.245	0.696	0.696	-0.046	0.213	-0.195	0.00
187056	3	6	F	-0.002	-0.134	-0.134	0.003	-0.052	-0.064	0.00
187056	4	6	F	0.005	-0.014	-0.014	-0.008	-0.006	-0.062	0.00
187057	1	8	F	-0.124	0.014	0.014	-0.081	-0.067	-0.108	0.00
187057	2	8	F	0.034	-0.014	-0.014	-0.030	-0.001	-0.006	0.00
187057	3	8	F	-0.068	0.016	0.016	-0.021	-0.023	-0.038	0.00
187057	4	8	F	-0.018	0.025	0.025	-0.025	-0.001	-0.012	0.00
187069	1	8	F	-0.058	-0.077	-0.077	0.008	-0.045	-0.125	0.00
187069	2	8	F	-0.045	-0.186	-0.186	-0.023	-0.090	-0.049	0.00
187069	3	8	F	0.026	0.040	0.040	0.020	0.031	0.020	0.00
187069	4	8	F	0.024	0.040	0.040	0.109	0.052	0.027	0.00
187082	1	5	F	-0.189	-2.000	-0.236	0.127	-0.083	-0.255	2.00
187082	2	5	F	-0.007	0.083	0.083	0.037	0.033	-0.029	0.00
187082	3	5	F	0.022	0.108	0.108	-0.009	0.046	0.091	0.00
187082	4	5	F	0.034	0.090	-0.162	-0.033	-0.058	0.102	-2.00
188006	1	8	F	0.009	-0.089	-0.089	0.046	-0.010	0.021	0.00
188006	2	8	F	0.028	-0.167	-0.167	-0.045	-0.055	-0.029	0.00

PID	AGE	YPT	YRT	MBA	TGA	TTA	THA	GBCA	AWA	APA
188006	3	8	F	0.031	-0.165	-0.165	-0.044	-0.060	-0.079	0.00
188006	4	8	F	-0.015	0.037	-0.272	0.080	-0.100	-0.013	-2.00
188018	1	2	S	-0.068	.	.	-0.023	-0.048	-0.099	0 00
188018	2	2	S	0.022	.	.	0.000	0.013	0.009	0.00
188018	3	2	S	-0.068	-0.341	-0.341	-0.129	-0.128	-0.132	0.00
188018	4	2	S	-0.045	-0.312	-0.312	-0.061	-0.099	-0.115	0.00
188030	1	7	F	0.054	-0 730	-0.730	-0.095	-0.156	-0.123	0.00
188030	2	7	F	-0.017	-0.130	-0.130	-0.205	-0.102	-0.129	0.00
188030	3	7	F	0.025	-0.224	-0.224	-0.082	-0.099	-0.110	0.00
188030	4	7	F	0.002	-0.281	-0.281	-0.052	-0.129	-0.080	0.00
188074	1	2	S	0.000	.	.	0.053	0.027	0.154	0.00
188074	2	2	S	0.000	-0.257	-0.257	-0 057	-0.064	-0 093	0.00
188074	3	2	S	-0.074	-0.044	-0.044	-0.020	-0.049	-0.038	0.00
188074	4	2	S	-0.008	-0.079	-0.079	-0.028	-0.032	0.008	0 00
188080	1	6	F	0.020	0.324	0.027	-0 023	0.009	-0.077	-2.00
188080	2	6	F	0.011	0.189	0 189	-0.058	0.055	0.018	0.00
188080	3	6	F	0.031	0.293	0.293	-0.061	0.108	0.136	0.00
188080	4	6	F	0.035	-0.014	-0.490	0.054	-0.224	0.076	-2.00
188085	1	4	F	0.070	-0.235	-0.235	0.075	0.015	-0.022	0.00
188085	2	4	F	-0 025	-0.078	-0.078	-0.023	-0.042	-0.102	0.00
188085	3	4	F	.	.	.	.		.	.
188085	4	4	F	0.069	0.053	-0.048	-0.017	0.005	0.014	-2.00
189005	1	6	F	0.009	0.173	0.173	-0.018	0 045	0.119	0.00
189005	2	6	F	-0.096	-0.415	-0.415	0.007	-0.159	-0.034	0.00
189005	3	6	F	0.055	-0.161	-0.161	-0.023	-0.043	0.017	0.00
189005	4	6	F	0.026	-0.074	-0.074	-0.019	-0.021	0.042	0.00
189006	1	4	F	0.032	0.188	0.188	-0.071	0.035	-0.043	0.00
189006	2	4	F	-0.061	0.029	0.029	0.007	-0.012	-0.021	0.00
189006	3	4	F	-0.012	0.039	0.039	0.086	0.030	0.000	0.00
189006	4	4	F	-0.002	-0.087	-0.087	-0.059	-0.048	0.039	0.00
189010	1	6	F	0.048	-0.165	-0.165	-0.015	-0.023	0.025	0.00
189010	2	6	F	0.056	0.055	0.055	0.098	0.067	0 060	0 00
189010	3	6	F	0.048	0.057	0.057	0.069	0.057	-0.040	0.00
189010	4	6	F	0.007	-0.149	-0.514	-0.029	-0.236	-0.041	-2.00
189013	1	3	F	0.079	-2.000	-2.000	0.259	0.083	0.000	0.00
189013	2	3	F	0.153	0.258	0.258	-0.011	0.129	0.109	0.00
189013	3	3	F	0.022	0.094	0.094	0.096	0.068	0.080	0.00
189013	4	3	F	-0.024	0 015	0.015	0.065	0.017	0.038	0.00
189017	1	8	F	-0.131	-0.101	-0.101	-0.008	-0.087	-0.133	0.00
189017	2	8	F	-0 068	-0.195	-0.195	-0.090	-0.126	-0.141	0.00
189017	3	8	F	-0.032	-0.171	-0.171	-0.014	-0.084	-0.106	0.00
189017	4	8	F	0.002	-0 020	-0.020	0.003	-0.006	-0.049	0 00
189021	1	7	F	0.839	0 652	0 652	0.224	0.575	0.840	0.00
189021	2	7	F	-0.033	-0.211	-0.211	-0.036	-0.097	-0.095	0 00
189021	3	7	F	0.027	-0.069	-0.069	-0.010	-0.019	-0.055	0 00
189021	4	7	F	-0 021	0.017	-0.045	-0.022	-0.031	-0.010	-2.00
189029	1	7	F	-0.018	-0.198	-0.198	0.085	-0.043	-0.030	0.00
189029	2	7	F	-0 009	-0.012	-0.012	0.031	-0.001	0.026	0 00
189029	3	7	F	0.016	-0.004	-0.004	-0.017	0.001	0.029	0.00
189029	4	7	F	-0.017	-0 036	-0.205	0.000	-0.094	0.014	-2.00
189044	1	6	F	-0 062	0.114	0.114	0.009	0.011	0.008	0.00
189044	2	6	F	0.080	0.072	0.072	0.030	0.063	0.122	0.00
189044	3	6	F	-0.013	0.000	0.000	-0.010	-0.007	-0.081	0 00

PID	AGE	YPT	YRT	MBA	TGA	TTA	THA	GBCA	AWA	APA
189044	4	6	F	-0.129	-0.321	-0.321	0.009	-0.164	-0.177	0.00
189050	1	9	F	0.089	-0.113	-0.113	0.194	0.061	0.024	0.00
189050	2	9	F	0.059	-0.094	-0.094	-0.013	-0.018	0.055	0.00
189050	3	9	F	-0.036	0.052	0.052	0.077	0.028	0.009	0.00
189050	4	9	F	-0.056	0.042	-0.136	0.107	-0.048	0.028	-2.00
189072	1	4	F	0.067	0.286	0.286	0.000	0.064	0.092	0.00
189072	2	4	F	0.019	0.325	0.325	-0.035	0.084	0.109	0.00
189072	3	4	F	0.014	0.079	0.079	0.041	0.042	0.053	0.00
189072	4	4	F	0.002	-0.124	-0.199	0.003	-0.066	-0.079	-2.00
189077	1	6	F	0.039	-0.052	-0.052	-0.029	-0.005	-0.031	0.00
189077	2	6	F	0.000	-0.175	-0.175	-0.194	-0.116	-0.090	0.00
189077	3	6	F	-0.009	-0.112	-0.112	0.033	-0.035	-0.090	0.00
189077	4	6	F	0.024	-0.130	-0.234	0.000	-0.077	-0.059	-2.00
189080	1	3	F	-0.011	-2.000	-2.000	0.327	0.050	0.096	0.00
189080	2	3	F	0.016	0.004	0.004	-0.042	-0.004	-0.058	0.00
189080	3	3	F	0.111	-0.244	-0.244	0.091	-0.026	-0.056	0.00
189080	4	3	F	-0.019	-0.036	-0.181	0.028	-0.066	0.012	-2.00
189090	1	4	F	-0.023	-0.022	-0.022	0.010	-0.011	-0.043	0.00
189090	2	4	F	0.190	0.143	0.143	-0.121	0.084	0.005	0.00
189090	3	4	F	-0.101	-0.063	-0.063	-0.060	-0.076	-0.109	0.00
189090	4	4	F	-0.055	-0.018	-0.018	-0.034	-0.036	-0.061	0.00
189091	1	4	F	-0.111	0.051	0.051	-0.050	-0.069	0.209	0.00
189091	2	4	F	0.051	0.161	0.161	0.016	0.075	0.131	0.00
189091	3	4	F	0.129	0.174	0.174	0.092	0.134	0.182	0.00
189091	4	4	F	0.034	0.055	-0.025	0.008	0.005	0.095	-2.00
189102	1	5	F	0.022	1.075	1.075	0.111	0.224	0.173	0.00
189102	2	5	F	-0.053	-0.274	-0.274	0.034	-0.088	-0.042	0.00
189102	3	5	F	0.100	-0.074	-0.074	0.051	0.027	0.062	0.00
189102	4	5	F	0.041	0.117	0.117	0.069	0.074	0.085	0.00
189103	1	7	F	-0.220	0.543	0.543	0.019	0.070	-0.057	0.00
189103	2	7	F	0.009	-0.076	-0.076	-0.007	-0.031	-0.043	0.00
189103	3	7	F	0.015	0.030	0.030	-0.151	-0.014	0.000	0.00
189103	4	7	F	0.203	-0.199	-0.242	-0.174	-0.097	-0.052	-2.00
189106	1	6	F	-0.003	-0.012	-0.012	0.034	0.006	-0.041	0.00
189106	2	6	F	-0.002	-0.021	-0.021	0.055	0.004	0.031	0.00
189106	3	6	F	0.041	0.003	0.003	0.015	0.019	0.071	0.00
189106	4	6	F	0.020	-0.150	-0.150	-0.016	-0.054	-0.026	0.00
189108	1	8	F	-0.054	0.079	0.079	0.099	0.034	0.047	0.00
189108	2	8	F	0.026	-0.171	-0.171	-0.078	-0.081	-0.008	0.00
189108	3	8	F	0.068	-0.546	-0.546	0.028	-0.175	-0.117	0.00
189108	4	8	F	-0.060	0.203	-0.044	0.064	-0.023	0.046	-2.00
189117	1	8	F	0.042	0.119	0.119	0.075	0.078	0.048	0.00
189117	2	8	F	0.042	-0.118	-0.118	-0.075	-0.052	-0.087	0.00
189117	3	8	F	0.023	0.001	0.001	0.008	0.010	0.047	0.00
189117	4	8	F	0.007	-0.012	-0.107	0.000	-0.045	0.056	-2.00
190030	1	6	F	-0.018	-0.417	-0.417	-0.091	-0.134	-0.124	0.00
190030	2	6	F	0.009	-0.141	-0.141	-0.019	-0.042	-0.055	0.00
190030	3	6	F	0.007	0.245	0.245	-0.029	0.081	0.049	0.00
190030	4	6	F	0.033	-0.069	-0.069	-0.018	-0.011	0.003	0.00
190035	1	6	F	-0.070	-0.021	-0.021	-0.043	-0.048	0.116	0.00
190035	2	6	F	-0.040	0.072	0.072	0.000	0.003	0.013	0.00
190035	3	6	F	-0.041	-0.058	-0.058	-0.052	-0.050	-0.046	0.00
190035	4	6	F	-0.017	-0.202	-0.202	-0.028	-0.090	-0.078	0.00

PID	AGE	YPT	YRT	MBA	TGA	TTA	THA	GBCA	AWA	APA
190039	1	8	F	0.000	0.004	0.004	-0.008	-0.001	0.000	0.00
190039	2	8	F	0.027	-0.074	-0 074	0.065	0.002	0.015	0.00
190039	3	8	F	0.027	-0.012	-0.012	-0.006	0.004	0.031	0.00
190039	4	8	F	0.016	-0.058	-0.142	0.003	-0.047	0.032	-2.00
190040	1	7	F	-0.083	0.318	0.318	-0.041	0.085	-0.018	0.00
190040	2	7	F	-0.016	-0.131	-0 131	-0.077	-0.079	-0.086	0.00
190040	3	7	F	-0.026	0.061	0.061	0.033	0.028	0.000	0.00
190040	4	7	F	-0.006	0.142	0.094	0.041	0.049	0 044	-2.00
190041	1	6	F	0 042	-0.043	-0 043	-0.030	0.001	0.033	0.00
190041	2	6	F	0.022	-0.025	-0.025	0.006	0.002	-0.052	0.00
190041	3	6	F	-0.049	-0.009	-0.009	-0.015	-0.025	-0.043	0.00
190041	4	6	F	-0.201	0.033	-0.600	0.113	-0.296	-0.103	-2.00
190043	1	9	F	-0.019	-0.209	-0 209	-0.144	-0.123	-0.026	0.00
190043	2	9	F	-0.016	-0.169	-0.169	-0.267	-0.148	-0.068	0.00
190043	3	9	F	-0.034	0.203	0.203	0.043	0.063	-0.075	0.00
190043	4	9	F	0.138	0.008	-0.879	-0.229	-0.415	.	-2.00
190055	1	2	S	-0.077	.	.	-0.189	-0.130	-0.114	0 00
190055	2	2	S	-0.006	-0.112	-0 112	-0.016	-0.025	-0.034	0.00
190055	3	2	S	-0.050	-0.323	-0.323	-0.230	-0.168	-0.162	0.00
190055	4	2	S	0.004	-0.208	-0.208	-0.039	-0.073	-0.106	0.00
190068	1	7	F	-0.036	0.243	0 243	0.008	0.054	0.039	0.00
190068	2	7	F	-0.027	-0 292	-0.292	0.084	-0.085	-0.052	0.00
190068	3	7	F	-0.076	0.207	0.207	0.103	0.077	0.117	0.00
190068	4	7	F	-0.029	0.415	0.415	0.029	0.145	0.195	0.00
190072	1	2	S	-0.098	.	.	-0.136	-0.117	-0.256	0.00
190072	2	2	S	0.022	-0.335	-0.335	0.029	-0.076	-0.145	0.00
190072	3	2	S	0.060	0.030	0.030	-0.072	0.010	0.036	0.00
190072	4	2	S	-0 002	-0.203	-0.203	-0.048	-0.078	-0.044	0.00
190073	1	2	S	-0 111		.	0 048	-0.046	-0.188	0.00
190073	2	2	S	0.059	0.086	0.086	0.036	0.057	0.061	0.00
190073	3	2	S	-0.007	-0.141	-0.141	-0.025	-0.044	0.018	0.00
190073	4	2	S	-0.025	0.110	0.110	0.022	0.029	0.045	0 00
190074	1	2	S	-0.065	.	.	0.022	-0 024	0.089	0.00
190074	2	2	S	0.052	0.216	0.216	0.118	0.105	0.157	0.00
190074	3	2	S	0.078	2.000	2.000	0.050	0.306	0.511	0.00
190074	4	2	S	-0.145	-2.000	-2.000	0 037	-0.571	-0.210	-2.00
190078	1	8	F	0 007	0 110	-0 051	-0.030	-0.021	-0.075	-2.00
190078	2	8	F	-0.077	-0.742	-0 742	-0.137	-0.252	-0.358	0.00
190078	3	8	F	-0.072	-0 085	-0.085	-0.006	-0.059	-0.107	0.00
190078	4	8	F	-0.129	-0.086	-0.346	0.024	-0.188	-0.036	-2.00
190083	1	5	F	-0 031	-0.139	-0.139	0.136	0.004	-0.083	0.00
190083	2	5	F	-0.034	0.472	0 472	0.035	0.114	-0.034	0.00
190083	3	5	F	0.011	-0.053	-0.053	0.024	-0.010	-0.005	0.00
190083	4	5	F	-0.086	0.037	0.037	-0.021	-0.026	-0.047	0.00
190087	1	6	F	0.000	-0.438	-0.438	0.033	-0.077	-0.048	0.00
190087	2	6	F	-0.008	-0.041	-0 041	-0.004	-0.017	-0.079	0 00
190087	3	6	F	0.020	0.022	0.022	0.020	0.021	0.037	0.00
190087	4	6	F	0.006	0.109	0.109	0.071	0.063	0.012	0.00
190091	1	3	F	-0.018	2.000	2.000	-0.161	-0.015	0.088	0.00
190091	2	3	F	0.017	0.636	0.636	-0.063	0.075	0.015	0.00
190091	3	3	F	0.008	-0.371	-0.371	0.022	-0.118	-0 064	0.00
190091	4	3	F	-0.016	-0.058	-0.058	-0.004	-0.029	-0.019	0.00
190098	1	6	F	-0 028	0.014	0.014	-0.026	-0.019	0.007	0.00

PID	AGE	YPT	YRT	MBA	TGA	TTA	THA	GBCA	AWA	APA
190098	2	6	F	-0.004	0.195	0.195	-0.019	0.046	0.007	0.00
190098	3	6	F	0.019	0.089	0.089	0.059	0.056	0.133	0.00
190098	4	6	F	0.028	0.034	-0.143	0.000	-0.052	0.089	-2.00

VITA

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